# **Evapotranspiration**

- **Evaporation** (E): In general, the change of state from liquid to gas
  - Here, liquid water on surfaces or in the very thin surface layer of the soil that evaporates directly to the atmosphere
- **Transpiration** (T): vapour loss from stomata in plant leaves
- **Evapotranspiration** (ET): net transfer (loss) of water vapour from wet surfaces (rivers, lakes, soil) & vegetation into the atmosphere...
  - each process difficult to measure separately... often combined as net evapotranspiration

# **Free-water loss**



FIGURE 4.2.1 Molecular exchange between liquid water and water vapor. Not all the molecules hitting the surface are captured, but some condense at a rate which is proportional to the vapor pressure of the moist air: molecules with enough energy vaporize at a rate determined by the surface temperature. Maidment (1993)

- Soil water that can be freed from the soil can proceed to the atmosphere in **two ways**:
- Evaporation Water in the soil evaporates directly into the atmosphere. Evaporation only affects the thin surface layer of soils, as the resistance to liquid water movement in soils is high
- Transpiration Plants provide an ideal conduit for the movement of water between soils and the atmosphere. Roots grow deep into the soil and can tap into water reserves far from the surface, providing a pathway between the deeper soil and the atmosphere



- The movement of water from the soil through plant and into the atmosphere is controlled by
  stomata, tiny holes on the back of leaves
- The atmosphere is usually drier than the air inside the stomata, thus there exists a water
  potential gradient (the potential in the outside air is more negative) causing the water
  move from the stomata into the atmosphere

- The negative water potential in the atmosphere is transferred to a **continuous column of liquid water** that begins in the root and ends in the leaf
- The tissue that the water passes through is called **xylem**, which provides an uninterrupted pathway for water movement
  - The tension is conducted out through the roots, and through contact between roots and soil, to the water adhering to soil particles
- This water column **must be continuous**. Any air gaps in the system will relieve the tension and stop the movement of water. Root surfaces must be in direct contact with the soil water film

- The actual **rate of flow** of water up through the plant, and thus from the soil to the atmosphere is a **function** of the **differences in water potential** between these two ends of the gradient and the **resistance to the flow**
- Resistance within the plant results mainly from **friction** between water and the walls of the xylem elements through which it passes
- The **force of gravity** also works against the rate of water movement up the stem
- During times of water stress, the guard cells lose water, reducing the turgor of the cells. As the guard cell loses turgor, the stomata will close, to further reduce the loss of water

#### **Transpiration loss**



# **Controlling factors for ET**

#### 1. Water:

- open bodies, intercepted, soil, plants
- 2. Energy:
  - major source is <u>short-wave</u> solar radiation
  - <u>long-wave</u> (sensible heats surfaces) &
  - <u>latent heat</u> (exchanged within air masses)
- **3.** Vapor pressure (humidity):
  - Difference between atmosphere & water source
  - pressure gradient controls rates of movement of  $H_2O$  molecules from moist surfaces to atm.
  - recall,  $e_a \le e^*$  or  $e_a \le e_s$
  - cannot exceed RH =100%



# **Controlling factors for ET**

#### **4. wind**:

- <u>turbulent</u> airflow above moist surfaces removes saturated air replacing it with unsaturated air  $(\downarrow e_a)$ 

#### 5. vegetation:

- transpiration is a product of photosynthesis
  - uses soil moisture
- rates controlled by  $e_a$
- also includes E<sub>i</sub> losses from plant canopies
- E from bare soil may actually »T from veg... why?



# **Physics of evaporation**

- Evaporation is a **diffusive** process ...a function of exchange across 'gradients'
  - energy gradient: latent- & sensible-heat exchange [E L<sup>-2</sup> T<sup>-1</sup>]
  - vapor pressure gradient: difference between e<sub>surface</sub> & e<sub>air</sub> (essentially a 'mass' gradient in [M L<sup>-1</sup> T<sup>-2</sup>])
  - windspeed (v<sub>a</sub>) & turbulent kinetic energy control vertical transport (removal) of H<sub>2</sub>O vapor

# Wind & turbulent energy effects

Described by **Fick's 1<sup>st</sup> Law**:  $E = K_e \cdot v_a \cdot (e_s - e_a)$ 

 $-K_{e}$  is a coefficient that describes the efficiency of vertical transport of water vapor via turbulent eddies

 $K_{\rm e} \equiv \frac{0.622\,\rho_{\rm a}}{P \cdot \rho_{\rm W}} \cdot \left| 6.25 \left( \ln \left[ \frac{z_{\rm m} - z_{\rm d}}{z_{\rm 0}} \right] \right)^2 \right|^{-1}$ 

 $-\rho_a = air density$ 

$$-\rho_{\rm w} =$$
 water density

$$- P =$$
atmospheric pressure

- $z_m$  is height windspeed V<sub>a</sub> & e<sub>a</sub> measured
- z<sub>d</sub> is zero-plane displacement height
- $-z_0$  is the aerodynamic roughness height

#### Latent heat exchange (LE)

• LE is 'lost' during vaporization  $(\lambda_v)$  & causes a reduction in  $T_s$  (i.e., cooling of surface) .... Example?

- if we measure  $\Delta LE$ , we know amount of energy avail. for evaporation

- $LE = \rho_{w} \cdot \lambda_{v} \cdot E = \rho_{w} \cdot \lambda_{v} \cdot K_{e} \cdot v_{a} (e_{s} e_{a})$ 
  - $\lambda_v$  latent heat of vaporization [E M<sup>-1</sup>] or MJ kg<sup>-1</sup>
  - as  $T_s$  increases,  $\lambda_v$  decreases:  $\lambda_v = 2.5 2.36 \times 10^{-3} T_s$
  - about 2.45 million joules are required to evaporate 1 kg of water at 20°C

# Sensible heat exchange (H<sub>S</sub>)

• upward sensible heat transfer, H<sub>S</sub> via turbulence:

$$H_{S} = K_{h} \cdot v_{a} (T_{s} - T_{a})$$
$$K_{h} \equiv C_{a} \cdot \rho_{a} \left[ 6.25 \left( \ln \left[ \frac{z_{m} - z_{d}}{z_{0}} \right] \right)^{2} \right]^{-1}$$

- $K_h$  coefficient describing **upward transfer** of  $H_S$  by wind
- C<sub>a</sub> is heat capacity of vapour-bearing air

# **Bowen Ratio**

> **Bowen Ratio** ( $\beta$ ) used to describe ratio of H<sub>S</sub>:LE

$$\beta \equiv \frac{H_s}{LE} = \frac{C_a \cdot \rho_a \cdot (T_s - T_a)}{0.622 \cdot \lambda_v \cdot (e_s - e_a)} = \gamma \cdot \frac{(T_s - T_a)}{(e_s - e_a)}$$

#### $\gamma$ = psychrometric constant

• describes the heat capacity, air density and latent heat of vapourization properties of the air mass

# **Measuring & modeling ET**

Five commonly used approaches:

- 1. Direct measurement of moisture loss
- 2. Radiation balance-based
- **3.** Aerodynamic based (mass transfer)
- 4. Combined radiation-aerodynamic
- 5. Temperature-based

## **Direct measurement**

 evaporation pan: E of exposed water from budget of W inputs & ∆ storage volume (V)

$$-\mathbf{E}_{\text{pan}} = \mathbf{P} - [\mathbf{V}_2 - \mathbf{V}_1]$$

- more appropriate for short vegetation & ground cover
- spatially limited, design biases, does not measure transpiration



Review: 1919, Sept.: 608.

## **Direct measurement**

 Lysimeter: Δ in weight of a control volume of soil proportionate to Δ in volume of moisture lost by surface evaporation & plant transpiration







(b) A giant 'floating' lysimeter containing a mature Douglas fir tree at Cedar River, Washington. The observer (centre left) is reading the manometer which monitors mass changes by the soil-tree monolith. Tensiometers are installed both inside and outside the lysimeter to ensure that similarity of moisture content is maintained. The brace in the foreground prevents rotation, and the tree is lightly 'guyed' to surrounding trees to prevent it falling over in high winds.



Gates, D.M. 1980. <u>Biophysical Ecology</u>. Springer-Verlag, Berlin and New York.

• We can describe the **net radiation** received by the Earth using the **Radiation Balance Equation**:

$$\mathbf{R}_{\mathrm{n}} = \mathbf{S}_{\mathrm{0}}(1.0 - \alpha) + \mathbf{L}_{\mathrm{n}}$$

Where:  $S_0$ : Shortwave radiation from the Sun

α: Albedo (describing reflected rad'n)

#### $L_n$ : Net longwave radiation

If  $R_n > 0$ , **net gain** of energy (daytime, summer)  $R_n < 0$ , **net loss** of energy (nighttime, winter)  $R_n = 0$ , then we have a **steady-state** condition

- After the Earth's surface receives R<sub>n</sub> radiative energy, the energy is **used in the following ways**:
- A portion of it will be used to **evaporate or transpirate** water from the liquid state to the gaseous state. This is called **latent heat (LE)** as the energy will be released when the gaseous water changes back to liquid state
- A portion of it will be used to heat the atmosphere, which is called sensible heat (H<sub>S</sub>)
- A portion of it will **pass through the Earth's surface** to **heat the soil** below (Q)
- A small fraction of the energy is used by leaves for **photosynthesis** and this **energy is stored** in the chemical bonds of carbohydrate produced by photosynthesis (A)

We can describe the way the net radiation received by the Earth's surface is partitioned using the Energy Balance Equation:

$$\mathbf{R}_{\mathbf{n}} = \mathbf{L}\mathbf{E} + \mathbf{H}_{\mathbf{S}} + \mathbf{H}_{\mathbf{G}} + \mathbf{A}$$

Where: LE: Latent heat

- H<sub>S</sub>: Sensible heat
- $H_G$ : Energy stored in the soil
- A: Energy stored in photosynthate
- How R<sub>n</sub> is distributed among the items on the right hand side is determined by the **ecosystem biophysical characteristics** and has major consequences for ecosystem development and functions

- $LE = R_S + R_L H_G H_S + H_A (\Delta H/\Delta t)$ 
  - $R_s = net short-wave radiation$
  - $R_L$  = net **long-wave** radiation
  - $H_G$  = net **ground heat** conduction (typically small)
  - $H_s$  = net **sensible heat** output to atmosphere
  - $H_A$  = net input associated with **inflow/outflow of water** (advected energy)
  - $\Delta H = \Delta$  heat stored in evaporating body (per unit area)
  - additional **photosynthetic energy** term (A) can be added... may amount to up to  $\underline{3\%}$  of  $R_N$

- Energy balance of a surface
  - $R_{\rm N} = H_{\rm G} + H_{\rm S} + LE$



Figure 1.11 Schematic summary of the fluxes involved in the radiation budget and energy balance of an 'ideal' site, (a) by day and (b) at night.



• You can calculate the ratio between sensible and latent heat fluxes, and this is known as the **Bowen Ratio** (β):

$$\beta = H / LE$$

• The sensible heat flux is often **difficult to measure**, but if you can estimate the Bowen Ratio, you can rewrite the **net radiation balance equation** in terms of latent heat:

$$R_n = H + LE + H_G$$
$$R_n = (\beta * LE) + LE + H_G$$
$$LE = (R_n - H_G) / (1 + \beta)$$



David Tenenbaum - EEOS 383 - UMass Boston

> Evaporation calculated via **Bowen ratio energy balance** method

$$LE = R_{N} - H_{S} - H_{G}$$

$$LE = \frac{(R_N - H_G)}{(1 + \beta)}$$

$$\mathbf{E} = \frac{(\mathbf{R}_{\mathrm{N}} - \mathbf{H}_{\mathrm{G}})}{\rho_{\mathrm{W}} \cdot \lambda_{\mathrm{V}} \cdot (1 + \boldsymbol{\beta})}$$

- Method seeks to apportion available energy between sensible and latent heat flux by considering their ratio  $\beta = \frac{H_s}{LE} = \gamma \cdot \frac{\Delta T}{\Delta e}$
- assumes neutral stability (buoyancy effects are absent) and steady state ( no marked shifts in radiation)



David Tenenbaum - EEOS 383 - UMass Boston

Subsurface heat flux for a lake



 $\mathbf{H}_{\mathrm{G}} = \mathbf{H}_{\mathrm{GL}} + \mathbf{H}_{\mathrm{GB}}$ 

 $H_G = \text{total subsurface heat flux (W m^{-2})}$  $H_{GL} = \text{lake heat storage (W m^{-2})}$  $H_{GB} = \text{heat conduction into lake bed (W m^{-2})}$ 

$$H_{GL} = C_{w} \times \frac{\Delta T}{\Delta t} \times \frac{V}{A}$$

V= lake volume 
$$(m^3)$$
 & A is lake area  $(m^2)$ 

 $\Delta T$  = change in temperature (°C) over time step

 $C_w$  = heat capacity of water (J m<sup>-3</sup> kg<sup>-1</sup>)

 $\Delta t \,(\text{sec})$ 

$$K_{\rm B}$$
 = bed thermal conductivity (W m<sup>-1</sup> °C<sup>-1</sup>)  
estimated from bed grain size

 $T_1$  is temperature (°C) at water bed interface and  $T_2$  at some depth below lake

 $\Delta z = \text{distance (m) between } T_1 \text{ and } T_2$ 

$$H_{GB} = -K_{B} \times \frac{(T_{1} - T_{2})}{\Delta z}$$

Subsurface heat flux for soil

$$H_{G} = C \times \frac{\Delta T}{\Delta t} \times \Delta z$$

$$\mathbf{C} = \mathbf{x}_{\mathrm{m}}\mathbf{C}_{\mathrm{m}} + \mathbf{x}_{\mathrm{om}}\mathbf{C}_{\mathrm{om}} + \mathbf{x}_{\mathrm{w}}\mathbf{C}_{\mathrm{w}} + \mathbf{x}_{\mathrm{a}}\mathbf{C}_{\mathrm{a}}$$

Where:

T = soil temperature

t = time

- z = depth of soil for which measurements are taken
- C = volumetric heat capacity

x = fraction of soil constituent (mineral (m), organic matter (om), water (W) and air (a))



## **Energy fluxes change over time**

Wetland adjacent to Lake Ontario



Fig. 2. Averages of the half-hourly measurements of net radiation ( $R_N$ ), and latent (LE), sensible ( $H_{st}$ ) and ground ( $H_{st}$ ) heat flux. The energy balance components were measured over the *Typha* canopy between 14 June and 6 August 1991.

# **Energy fluxes change over time**

**Experimental Field in California** 



Hornberger et al. 1998. <u>Elements of Physical Hydrology</u>. The Johns Hopkins University Press, Baltimore and London.

## **Energy fluxes change over time**



Figure 1.10 (a) Energy balance components for 30 May 1978 with cloudless skies at Agassiz, B.C. (49°N) for a moist, bare soil, and (b) temperatures at the surface, in the air at a height of 1.2 m and in the soil at a depth of 0.2 m (after Novak and Black, 1985). The following table gives the energy totals for the day (MJ m<sup>-2</sup> day<sup>-1</sup>).

Energy balance for a moist, bare soil on May 30, 1978 at Agassiz, BC.

Daily summary  $R_N = 18.0$   $H_S = 2.3$  LE = 13.4  $H_G = 2.3$ units in MJ m<sup>-2</sup> day<sup>-1</sup> note: 1 W = 1 J s<sup>-1</sup>

• Semi-empirical approach requires measurements on one level above surface

**Priestly & Taylor** (1972):

$$PET = \alpha \cdot \frac{s}{s + \gamma} \cdot \frac{(R_N - H_G)}{\rho_w \cdot \lambda_v}$$

where:

- PET is **potential evapotranspiration** (mm per time)
- $s = (e_s^* e_a^*)/(T_s^- T_a)...$  describes **gradient** of e\* vs. T at a given air temperature
- $\alpha$  is an empirically derived **evaporability factor** (usually 1.26)

# **Aerodynamic Profile Method**

Unmodified method applies to the following **restricted conditions**:

- i) neutral stability buoyancy effects absent
- ii) **steady state** no marked shifts in radiation or wind fields during observation periods
- iii) constancy of fluxes with height no vertical divergence or convergence

iv) similarity of all transfer coefficients

under these conditions the logarithmic wind profile is valid and the wind gradient is found to be **inversely proportional to the height above a surface** 



Figure 2.10 The wind speed profile near the ground including: (a) the effect of terrain roughness (after Davenport, 1965), and (b) to (e) the effect of stability on the profile shape and eddy structure (after Thom, 1975). In (e) the profiles of (b) to (d) are re-plotted with a natural logarithm height scale.

# **Aerodynamic Profile Method**

$$E = -\rho_{a} \cdot \kappa^{2} \cdot \frac{(u_{2} - u_{1}) \cdot (q_{2} - q_{1})}{(\ln z_{2}/z_{1})^{2}} \cdot (\phi_{m} \times \phi_{v})^{-1}$$

where:

κ is the von Karman constant (0.4) u is the mean windspeed (m s<sup>-1</sup>) at height z q is the mean specific humidity (g kg<sup>-1</sup>) z is the measurement height above surface 1= lower and 2 = upper

 $\phi_m$  and  $\phi_v$  are stability corrections for momentum and water vapor



# **Combined approaches**

- Penman (1948) developed a method considering the factors of both energy supply and turbulent transport of water vapor from an evaporating surface
- Requires meteorological measurements at **only 1 level**
- in the combination method LE is **calculated as the residual** in the energy balance equation with sensible heat flux estimated by means of **an aerodynamic equation**
- widely used for estimating potential evapotranspiration
- original method designed to estimate evaporation from open-water or well-watered surfaces
  - e.g., lake, pond, and wetlands

# **Types of ET**

#### TABLE 7-1

#### Classification of Types of Evapotranspiration

<b>Evapotranspiration Type</b>	Type of Surface	Availability of Water to Surface	Stored Energy Use	Water-Advected Energy Use
Free-water evaporation <sup>a</sup>	Open water	Unlimited	None	None
Lake evaporation	Open water	Unlimited	May be involved	May be involved
Bare-soil evaporation	Bare soil	Limited to unlimited	Negligible	None
Transpiration	Leaf or leaf canopy	Limited	Negligible	None
Interception loss	Leaf or leaf canopy	Unlimited	Negligible	None
Potential evapotranspiration	Reference crop <sup>b</sup>	Limited to air, unlimited to plants	None	None
Actual evapotranspiration	Land area <sup>c</sup>	Varies in space and time	Negligible	None

#### <sup>a</sup>Also called **potential evaporation**.

<sup>b</sup>Usually a complete ground cover of uniform short vegetation (e.g., grass); discussed further in Section 7.7.1.

<sup>c</sup>May include surface-water bodies and areas of bare soil.

# **Combined** approaches

#### **Penman (1948):**

$$PET = \frac{s \cdot (R_{N} - H_{G}) + \frac{C_{a} \cdot (e_{s} - e_{a})}{r_{a}}}{\rho_{W} \cdot \lambda_{V} \cdot (s + \gamma)}$$



$$r_{a} = \frac{\left[\ln(z - d)/z_{O}\right]^{2}}{\kappa^{2} \cdot u_{z}}$$

**Aerodynamic resistance**,  $r_a$ , describes the resistance from the water or vegetation upward and involves friction of air flowing over water or vegetative surface

 $r_a = aerodynamic resistance (s m^{-1})$ 

$$u_z = is wind speed (m s^{-1}) at elevation z (m)$$

 $\kappa$ = van Karman's constant (0.4)

$$\kappa z_0 = \text{roughness length}(m)$$

$$\kappa d = zero plane of displacement$$



David Tenenbaum - EEOS 383 - UMass Boston

# **Actual evapotranspiration (ET)**

- where PET > available moisture, ET is **water-limited** 
  - e.g., hot arid regions
  - ET also limited by insufficient energy to fuel the process (i.e., ET = PET)... e.g., arctic environments
- how to estimate ET?
  - water budget approach  $ET = W / ([1+(W/PET)^2]^{1/2})$
  - soil-moisture function  $ET = F(\theta_{rel}) \bullet PET$ 
    - $F(\theta_{rel})$  is water infiltrated to <u>relative water content</u> ( $\theta_{rel}$  in mm) where  $\theta_{rel} = (\theta - \theta_{pwp} / \theta_{fc} - \theta_{pwp})$  where 'pwp' = permanent wilting point & 'fc' = field capacity
  - weighing lysimeter $\Delta$  in weight of a control volume of soil<br/>proportionate to  $\Delta$  in volume of moisture lost<br/>by surface evaporation & plant transpiration

# **Combined approaches**

• **Penman-Monteith equation** common for ET from a vegetated land surface

$$PET = \frac{s \cdot (\mathbf{R}_N - \mathbf{G}) + \frac{\rho_a c_a \cdot (e_s - e_a)}{r_a}}{\rho_w \cdot \lambda_v \cdot [s + \gamma \cdot (1 + r_c / r_a)]}$$

$$r_c = \frac{r_i}{LAI_{active}}$$

where:

 $r_c = canopy resistance (s m^{-1})$ 

 $r_i$  = bulk stomatal resistance of the well-illuminated leaf (s m<sup>-1</sup>)

 $LAI_{active} = active (sunlit) leaf area index (m<sup>2</sup> leaf area per m<sup>2</sup> soil surface)$ 

# **Temperature-based**

•Thornthwaite (1948) related PET to monthly temp & daylength

$$PET = 16 \times \left(\frac{h}{12}\right) \times \left(\frac{N}{30}\right) \times \left(\frac{10 \times T_{ma}}{I}\right)^{a}$$

$$I = \sum_{i=1}^{12} \left(\frac{T_{ma}}{5}\right)^{1.5}$$

 $a = 0.49 + 0.0179 - 0.000771 \times I^2 + 0.000000675 \times I^3$ 

where:

PET = potential evapotranspiration (mm mo<sup>-1</sup>)

h = day length hours

N = number of days in the month

 $T_{ma}$  = mean monthly air temperature (°C)

I = annual heat index

### **Temperature-based**

#### Hamon (1963) see Dingman (2002)

PET = 29.8 D 
$$\left[ \frac{e_a^*(T_a)}{T_a + 273.2} \right]$$

where:

PET = potential evapotranspiration (mm d<sup>-1</sup>) D = hours of sunshine in 12 hour units (hr)  $T_a = air temperature (°C)$ 

$$e_{a}^{*}(T_{a}) = 0.611 \exp\left[\frac{17.27T_{a}}{T_{a}+237.3}\right]$$



#### Surface water/energy budget coupling over heterogeneous terrain



 $LE = f_{veg} LE_{veg} + (1 - f_{veg}) LE_{soil}$  $LE = f(R_n, T, g_c, g_a, g_{soil}, VPD)$  $g_a = f(canopy structure, wind, ...)$  $g_c = f(soil water, VPD, PAR, T, LAI)$  $g_{soil} = f(soil water, ...)$ 

 $T_s$  lower with greater LE (evaporative cooling) as a function of soil water (other factors), greater canopy cover (higher NDVI)

T<sub>s</sub> and NDVI estimated by a set of operational remote sensors