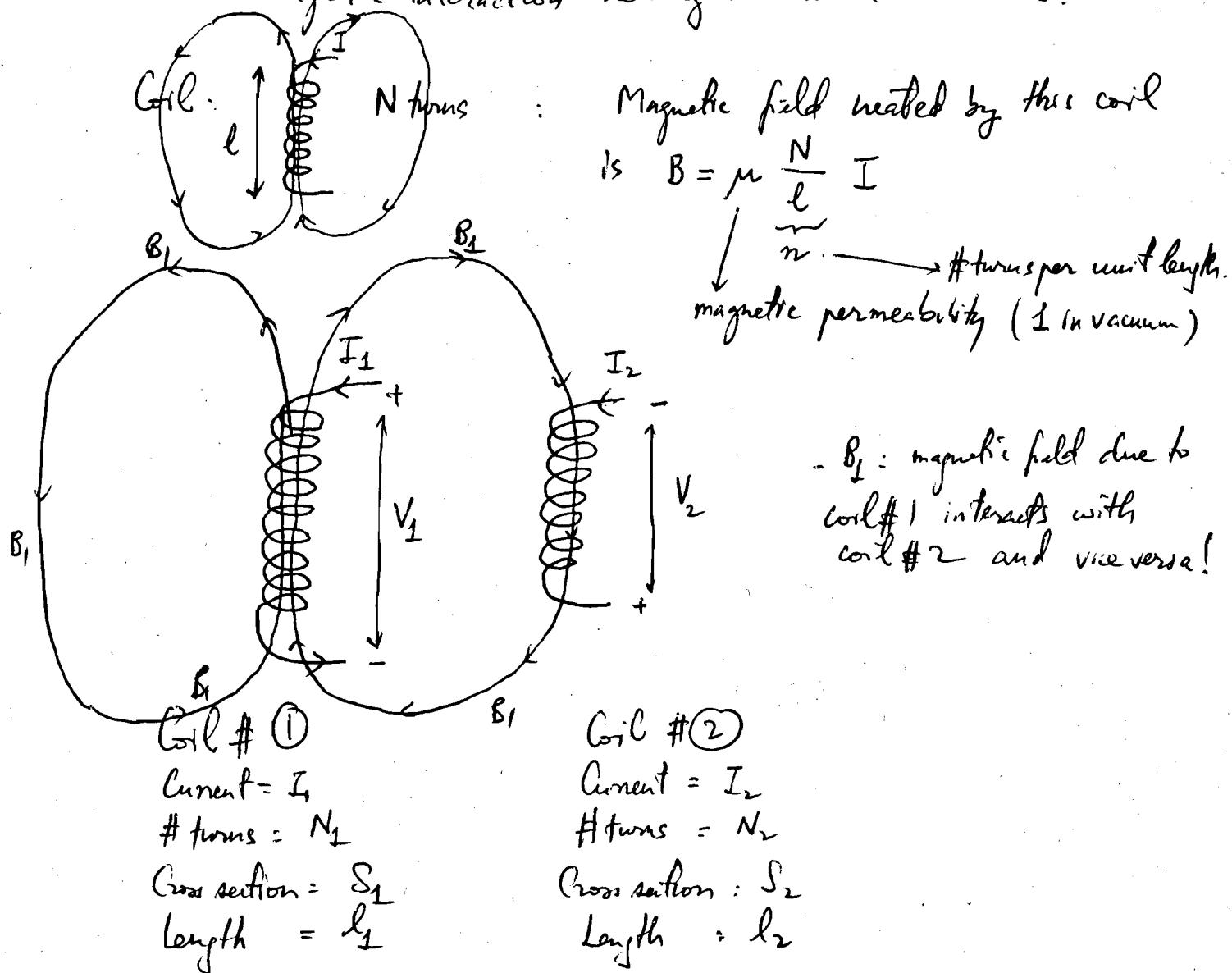


Magnetically Coupled Circuits

(7th ed : Ch. 8 or 8th ed : Ch 10)

So far inductance L is actually self-inductance : we haven't considered magnetic interaction, leading to mutual inductance.



Magnetic flux: $\phi = \vec{B} \cdot \vec{S}$ (larger field and larger cross section \rightarrow larger flux)

Faraday's law: $\underbrace{\text{induced e.m.f.}}_{\text{potential}} = \frac{d\phi}{dt}$ coil not expanding

$$V = \frac{d\phi}{dt} = \frac{d}{dt} (B \cdot S) = S \frac{dB}{dt} = S \frac{d}{dt} (\mu n I)$$

$$V = \frac{S_{\text{un}}}{L} \frac{dI}{dt}$$

This is what we have been using so far.

$$V_1 = L_1 \frac{dI_1}{dt}$$

one coil, one current.

→ Two coils, two currents I_1 & I_2 :

$$V_1 = L_1 \frac{dI_1}{dt} + M \frac{dI_2}{dt}$$

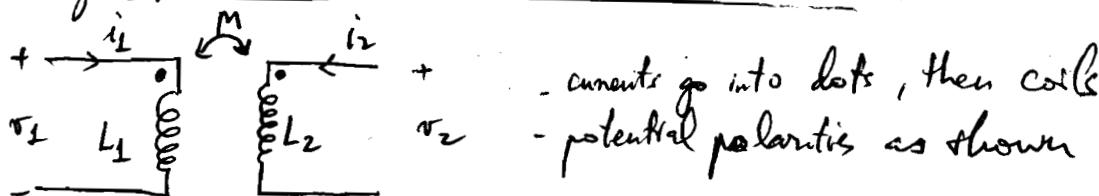
self-inductance mutual-inductance

due to magnetic interaction b/w the two coils.

$$\text{Similarly: } V_2 = L_2 \frac{dI_2}{dt} + M \frac{dI_1}{dt} \quad (M_{12} = M_{21})$$

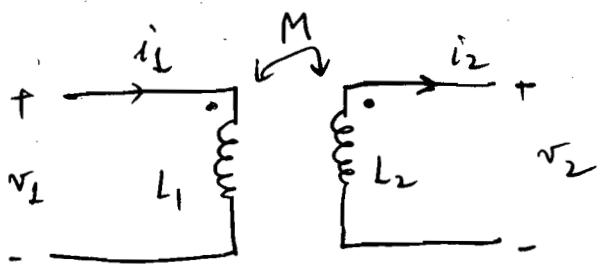
Conclusion: for our purposes of doing circuit analysis, the implication of including magnetic interaction is the consideration of one extra term with the correct sign: using the "dot convention"

Correct sign for the mutual inductance term (dot convention)



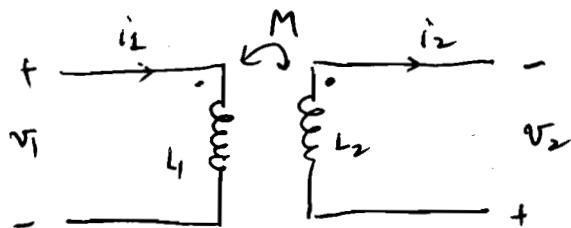
$$\left. \begin{aligned} V_1 &= L_1 \frac{di_1}{dt} + M \frac{di_2}{dt} \\ V_2 &= L_2 \frac{di_2}{dt} + M \frac{di_1}{dt} \end{aligned} \right\} \text{for phasors} \quad \left. \begin{aligned} \hat{V}_1 &= j\omega L_1 \hat{I}_1 + j\omega M \hat{I}_2 \\ \hat{V}_2 &= j\omega L_2 \hat{I}_2 + j\omega M \hat{I}_1 \end{aligned} \right\}$$

$\rightarrow \hat{V}_e^{\text{int}}$
 $\rightarrow \hat{I}_e^{\text{int}}$

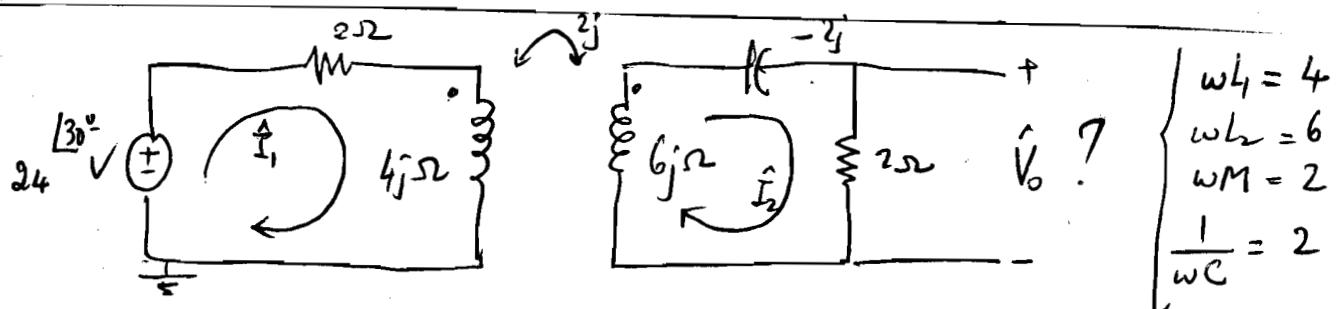


- one current goes into dot, then coil
- one current leaving dot
- polarities as shown

$$\left. \begin{aligned} v_1 &= L_1 \frac{di_1}{dt} - M \frac{di_2}{dt} \\ v_2 &= -L_2 \frac{di_2}{dt} + M \frac{di_1}{dt} \end{aligned} \right\} \xrightarrow{\text{phasor}} \left. \begin{aligned} \hat{v}_1 &= j\omega L_1 \hat{I}_1 - j\omega M \hat{I}_2 \\ \hat{v}_2 &= -j\omega L_2 \hat{I}_2 + j\omega M \hat{I}_1 \end{aligned} \right\}$$



$$\left. \begin{aligned} v_1 &= L_1 \frac{di_1}{dt} - M \frac{di_2}{dt} \\ v_2 &= L_2 \frac{di_2}{dt} - M \frac{di_1}{dt} \end{aligned} \right\} \xrightarrow{\text{phasor}} \left. \begin{aligned} \hat{v}_1 &= j\omega L_1 \hat{I}_1 - M j\omega \hat{I}_2 \\ \hat{v}_2 &= j\omega L_2 \hat{I}_2 - M j\omega \hat{I}_1 \end{aligned} \right\}$$



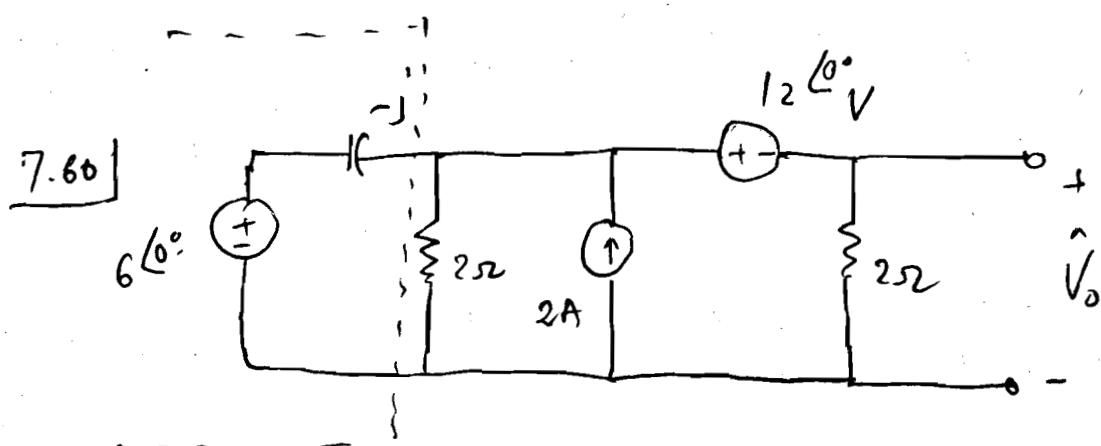
Loop analysis:

$$1) \quad 24^{\angle 30^\circ} = 2\hat{I}_1 + 4j\hat{I}_1 \underbrace{- 2j\hat{I}_2}_{\text{New!!}}$$

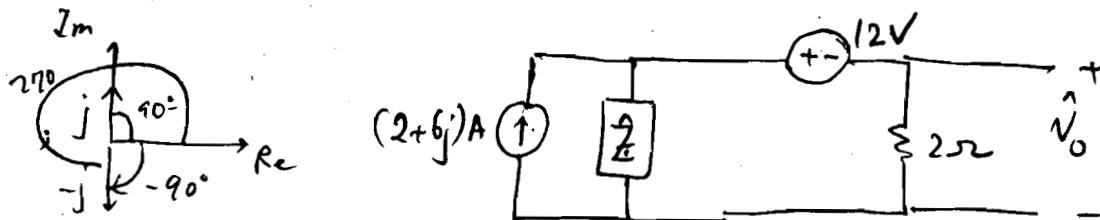
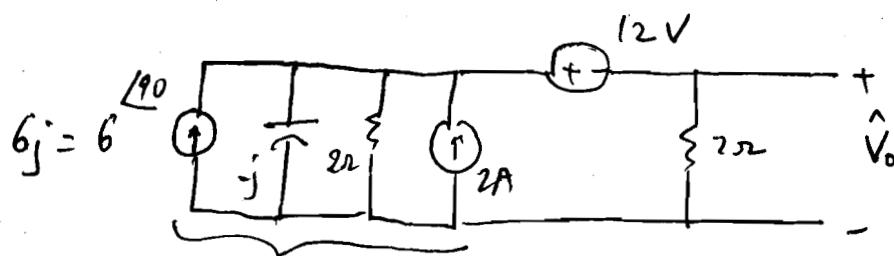
$$2) \quad 0 = 6j\hat{I}_2 \underbrace{- 2j\hat{I}_1}_{\text{New!!}} + (2 - 2j)\hat{I}_2$$

$$25/\text{HW3} \quad \hat{V}_0 = 2\hat{I}_2 = 5.36^{\angle 34.3^\circ} \text{ V}$$

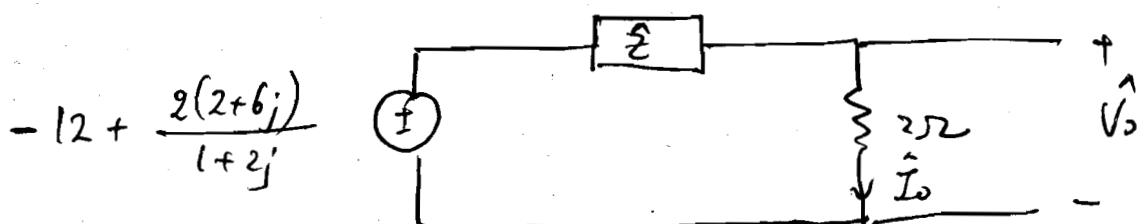
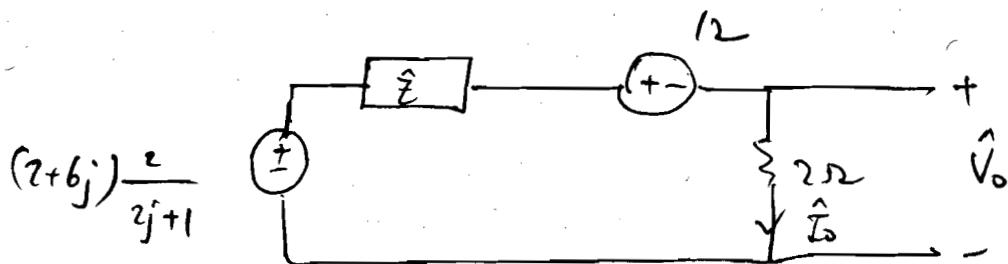
polar form



source exchange



$$\hat{Z} = 2 \parallel -j = \frac{-2}{2-j} = \frac{2}{2j+1}$$

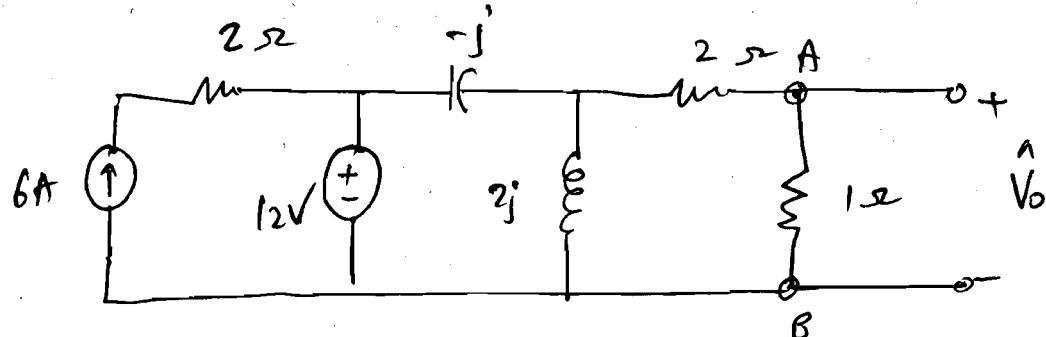


Voltage div: $\hat{V}_o = \left[-12 + \frac{2(2+6j)}{1+2j} \right] \frac{2}{2 + \frac{2}{2j+1}}$

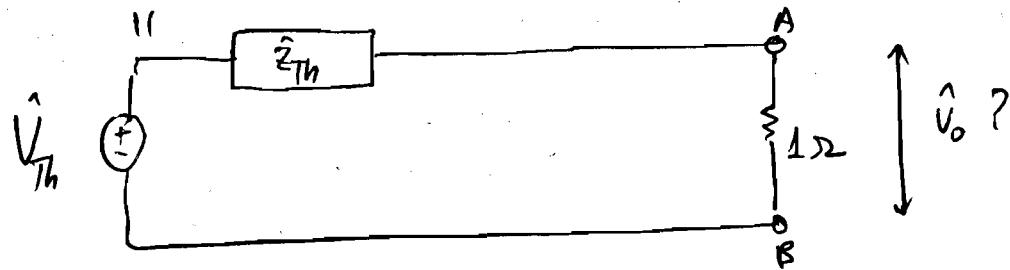
$$= \left[-12(1+2j) + 2(2+6j) \right] \frac{2}{2+4j+2}$$

$$\begin{aligned}
 \hat{V}_o &= \left[-8 - 12j \right] \frac{2}{4(1+j)} \\
 &= \frac{(-2 - 3j)2}{1+j} = 2 \angle 180^\circ \frac{(2+3j)}{1+j} \\
 &= 2 \angle 180^\circ \frac{\sqrt{13}}{\sqrt{2}} \angle \tan^{-1} \frac{3}{2} \quad 56^\circ = 5.1 \angle 191.3^\circ \quad \checkmark
 \end{aligned}$$

7.63

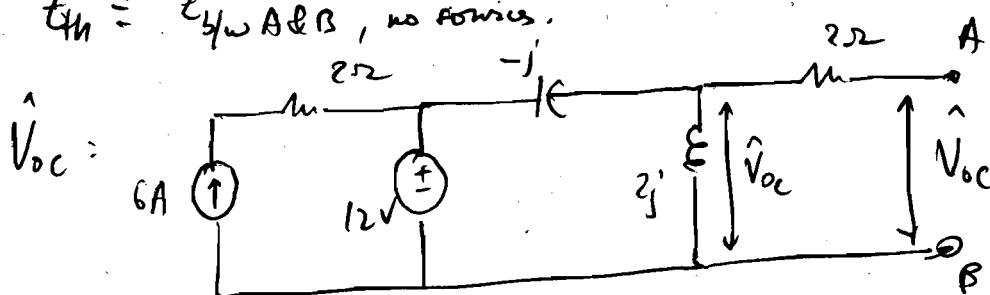


Use
Thévenin's
equivalent.

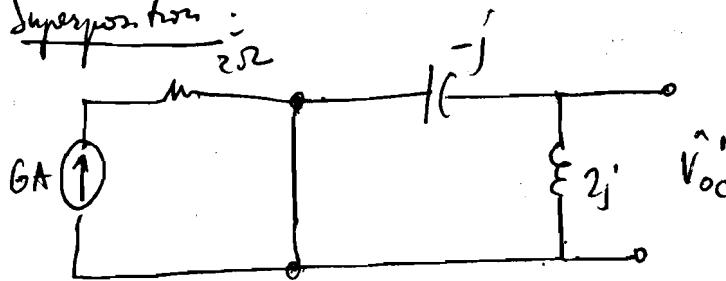


$$\hat{V}_{Th} = \hat{V}_{o.c. \text{ b/w } A \& B}$$

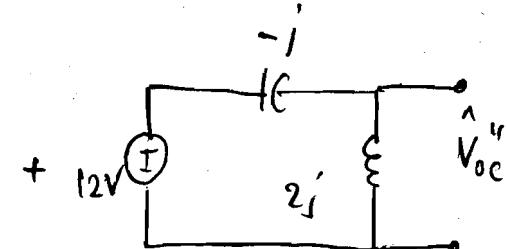
$$\hat{Z}_{Th} = \hat{Z}_{b/w A \& B, \text{ no sources.}}$$



Superposition:



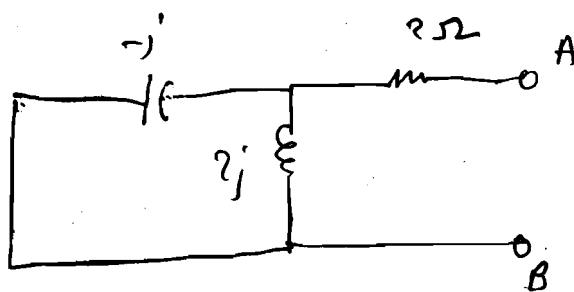
$$\hat{V}_{oc}' = 0$$



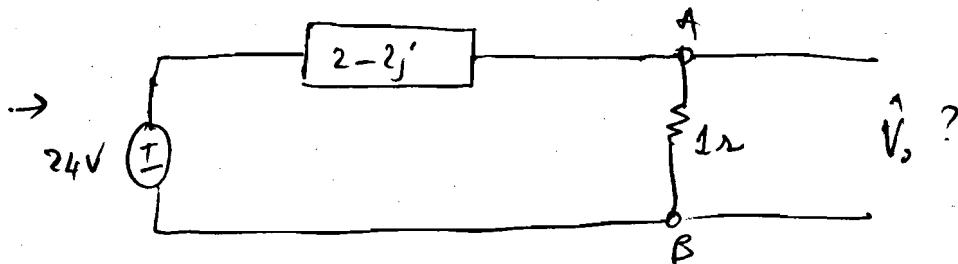
$$\hat{V}_{oc}'' = 12 - \frac{2j}{1j} = 24V$$

$$\hat{V}_{th} = 24V$$

$$\hat{Z}_{th} =$$



$$\begin{aligned}\hat{Z}_{th} &= 2 + \frac{2j(-j)}{2j-j} \\ &= 2 + \frac{2}{j} \\ &= 2 - 2j\end{aligned}$$



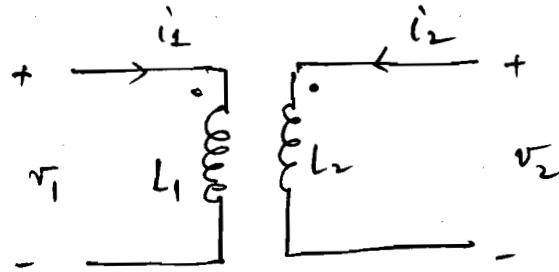
$$V_o = 24 \cdot \frac{1}{3-2j} = \frac{24}{\sqrt{13} \left[-\tan^{-1} \frac{2}{3} \right]} = \frac{24}{\sqrt{13}}$$

$$= 6.66 \angle 33.69^\circ V$$

(solution is good) -

Mutual inductance (Cont.)

Energy analysis:



$$\text{Power } P = \text{energy per unit time} \rightarrow E = \int P(t) dt$$

We look at two time intervals:

$$0 \longrightarrow t_1 \longrightarrow t_2$$

$$i_1 : 0 \longrightarrow I_1 \xrightarrow[\text{(max)}]{\text{const}} I_1$$

$$i_2 : 0 \xrightarrow{\text{const.}} 0 \longrightarrow I_2 \xrightarrow[\text{(max)}]{\text{const.}} I_2$$

$$\text{At any time: } P(t) = i_1 v_1 + i_2 v_2$$

$$= i_1(t) \left[L_1 \frac{di_1}{dt} + M \frac{di_2}{dt} \right] + i_2(t) \left[L_2 \frac{di_2}{dt} + M \frac{di_1}{dt} \right]$$

$$E = \underbrace{\int_0^{t_1} P(t) dt}_{i_2 \text{ const} \neq 0} + \underbrace{\int_{t_1}^{t_2} P(t) dt}_{i_2 = I_1 \text{ const}} = \int_0^{t_1} L_1 i_1 \frac{di_1}{dt} dt + \int_{t_1}^{t_2} \left(I_1 M \frac{di_2}{dt} dt + L_2 i_2 \frac{di_2}{dt} dt \right)$$

$$E = L_1 \int_0^{I_1} i_1 di_1 + M I_1 \int_0^{I_2} di_2 + L_2 \int_0^{I_2} i_2 di_2$$

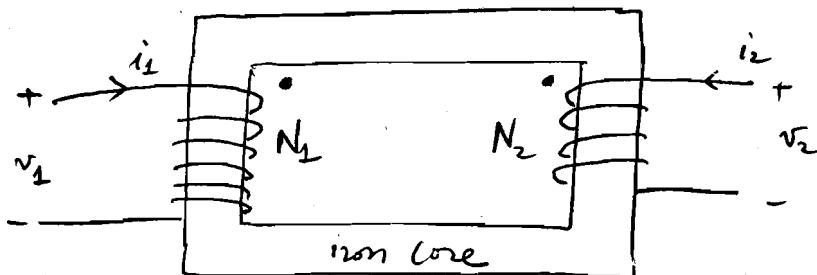
$$= L_1 \frac{I_1^2}{2} + M I_1 I_2 + L_2 \frac{I_2^2}{2} \rightarrow E = \frac{1}{2} L_1 I_1^2 + \frac{1}{2} L_2 I_2^2 + M I_1 I_2$$

mutual
magnetic
induction

Ideal Transformer :

Two coils + iron core

To change the voltage using different number of turns



coils

$$\left\{ \begin{array}{l} v_1 = N_1 \frac{d\phi_1}{dt} \\ v_2 = N_2 \frac{d\phi_2}{dt} \end{array} \right.$$

$\phi_1 = \phi_2$ (iron core)

$$\frac{v_1}{v_2} = \frac{N_1}{N_2}$$

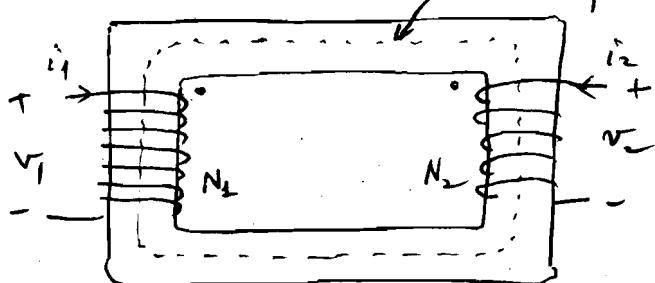
Faraday's Law : change of magnetic flux w.r.t. time \rightarrow induced voltage.

Iron core: similar to a short-circuit for electrons (electric fields), the iron core channels all magnetic field lines
 \rightarrow can find the flux: $\Phi_1 = \Phi_2$

Ampere's Law:

$$\oint \vec{H} \cdot d\vec{l} = i_{\text{enclosed by loop}} = i_1 N_1 + i_2 N_2$$

ampersian loop.



$$\vec{B} = \mu \vec{H}$$

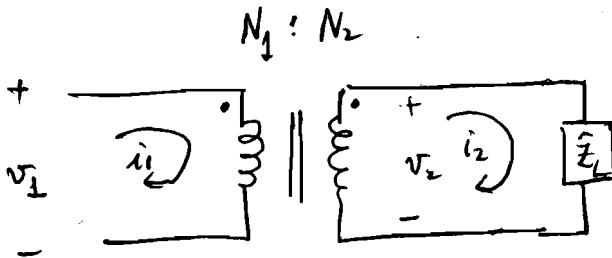
m. induction m. permeability

$\downarrow \mu$ 1 for vacuum
 ∞ for iron core

If $\mu = \infty \Rightarrow$ for a finite value for B
 H has to be 0 $\rightarrow 0 = i_1 N_1 + i_2 N_2$

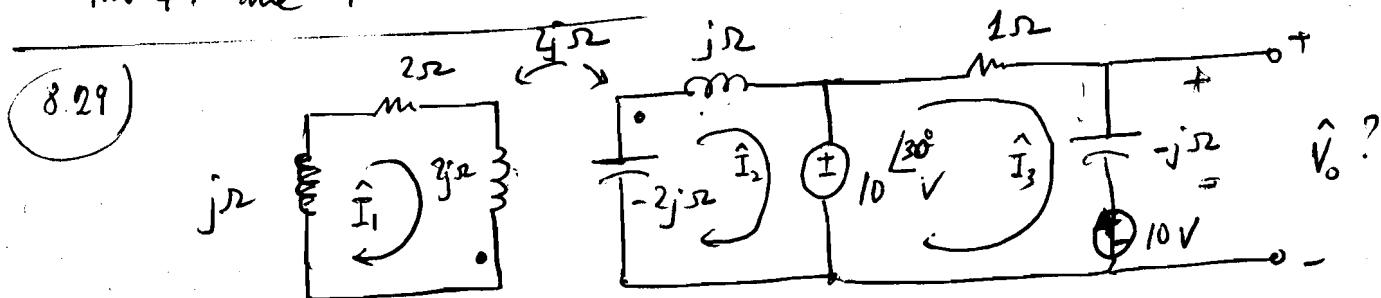
$$\frac{i_2}{i_1} = -\frac{N_2}{N_1}$$

Ideal transformer in a circuit



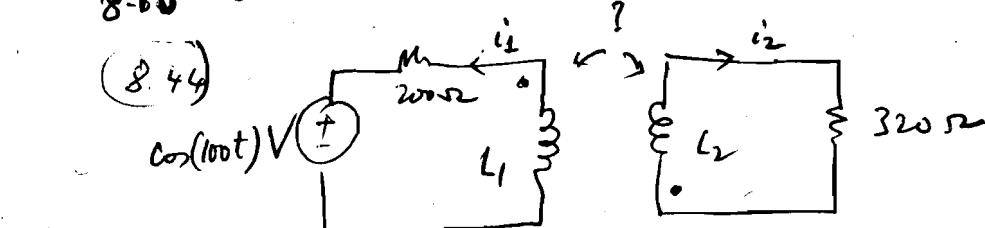
$$\left\{ \begin{array}{l} \frac{v_1}{v_2} = \frac{N_1}{N_2} \\ \frac{i_1}{i_2} = \frac{N_2}{N_1} \end{array} \right.$$

HW 4: due 3/13



$$\begin{aligned} 1) \quad & 3j\hat{I}_1 + 2\hat{I}_1 - \hat{I}_2 j = 0 && (\hat{I}_1 \text{ goes into } L_1 \text{ then dot} \\ 2) \quad & -j\hat{I}_2 + 10^{30^\circ} - j\hat{I}_1 = 0 && (\hat{I}_2 \text{ goes into dot then } L_2) \\ 3) \quad & -10^{30^\circ} + \hat{I}_3(1-j) + 10 = 0 \rightarrow \hat{I}_3 = \frac{-10 + 10^{30^\circ}}{1-j} = 3.66 \angle 150^\circ \end{aligned}$$

$$\hat{V}_0 = 3.66 \angle 150^\circ - 10 \angle 90^\circ \rightarrow \hat{V}_0 = \hat{I}_3(-j) + 10 \rightarrow (\text{Eliminate } \hat{I}_1 \text{ & } \hat{I}_2)$$



$$k^2 = \frac{M^2}{L_1 L_2} : \text{coupling coeff.}$$

$$k = 0.8; L_1 = L_2 = 4H$$

Then solve for $\hat{I}_2 =$