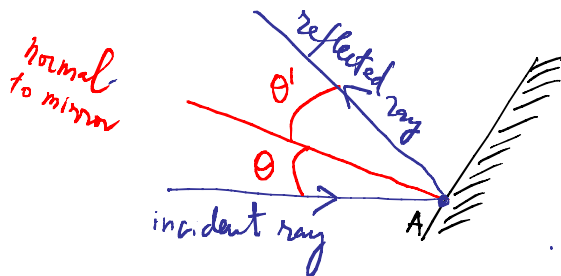


# Ch 30 Reflection & Refraction

Geometrical Optics: (Ch 30 & 31) uses geometry to solve for directions of light rays which travel in straight paths

Physical Optics: (Ch 32) when these rays travel through small openings  $\sim$  wave length  $\lambda$

Law of Reflection:  $\theta' = \theta$  (Reflected angle = incident angle)



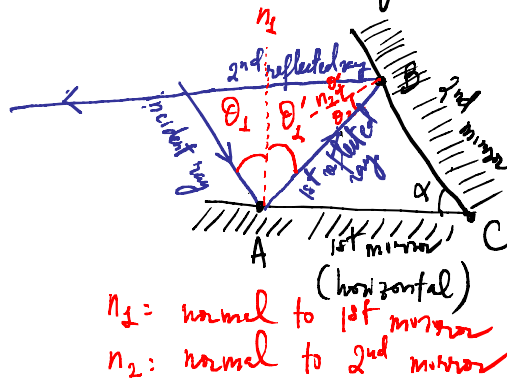
light doesn't travel through this side of mirror!

$\rightarrow$  Normal direction: perpendicular to mirror @ incident point A

$\hookrightarrow$  Angles are defined wrt. Normal directions  $\left\{ \begin{array}{l} \text{Incident angle } \theta \\ \text{Reflected angle } \theta' \end{array} \right.$

$\rightarrow$  Law of Reflection also applies to a system of mirrors:

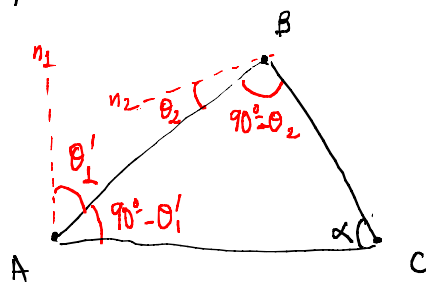
Law of Reflection  $\left\{ \begin{array}{l} \theta'_1 = \theta_1 \\ \theta'_2 = \theta_2 \end{array} \right.$



Goal: to determine  $\theta'_2$  (direction of outgoing ray)

$\hookrightarrow$   $\left\{ \begin{array}{l} \text{(i) law of reflection} \\ \text{(ii) Geometry} \end{array} \right.$

$\alpha$  will affect  $\theta'_2 \Rightarrow$  look at triangle  $\triangle ABC$



Geometry  $\rightarrow 90^\circ - \theta'_1 + 90^\circ - \theta_2 + \alpha = 180^\circ$   
 $\alpha - \theta'_1 - \theta_2 = 0$

$\theta_2 = \alpha - \theta'_1$

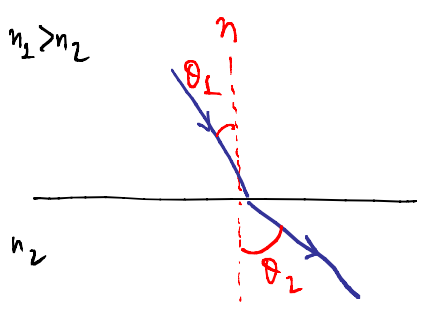
$\Rightarrow \theta'_2 = \alpha - \theta_1$

Law of Reflection:  $\theta'_2 = \theta_2 = \alpha - \theta'_1 = \alpha - \theta_1$

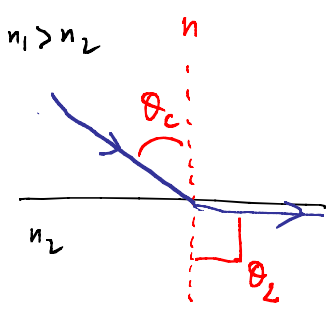


# Law of Refraction or Snell's Law & Critical Angle $\theta_c$ when $n_1 > n_2$

$\theta \geq \theta_c \leftrightarrow$  total internal reflection:



$\theta_2 < \theta_1$

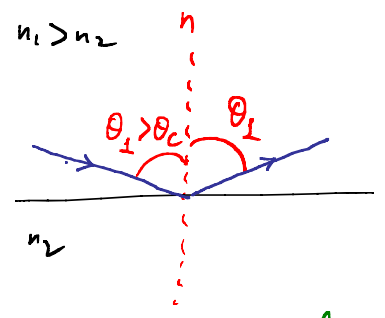


at certain  $\theta_1 = \theta_c$   
 $\theta_2 = 90^\circ$  or refracted ray is parallel to boundary b/w two media

Technically there is no refraction as the "refracted ray" doesn't travel in medium 2

↓ Light ray stays in medium 1  
 → "total internal reflection"

(Incident ray stays internally within medium 1)



Total internal reflection for  $\theta_1 > \theta_c$

Snell's Law:  $\left\{ \begin{matrix} \theta_1 = \theta_c \\ \theta_2 = 90^\circ \end{matrix} \right\} \rightarrow n_1 \sin \theta_c = n_2 \frac{\sin 90^\circ}{1}$

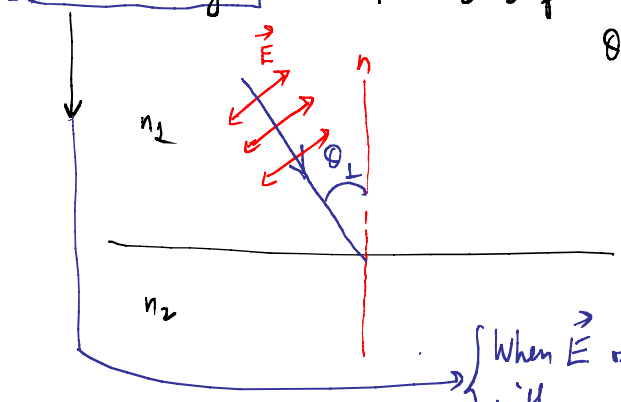
$\theta_c = \sin^{-1} \left( \frac{n_2}{n_1} \right)$

Note: only defined when  $n_2 < n_1$  or  $n_1 > n_2$  (from higher index to lower index!)

# Brewster's angle or polarizing angle:

Critical angle:  $\left\{ \begin{array}{l} \theta_i > \theta_c \\ (n_1 > n_2) \end{array} \right\} \rightarrow$  all rays are reflected, none is refracted  
 $\theta_c = \sin^{-1} \left( \frac{n_2}{n_1} \right)$

**Brewster's angle:**  $\theta_i = \theta_B$  or  $\theta_p \rightarrow$  all rays are refracted, none is reflected  
 $\theta_p$  or  $\theta_B = \tan^{-1} \left( \frac{n_2}{n_1} \right)$



When  $\vec{E}$  oscillates  $\perp$  to incident ray and in plane with page as shown and if  $\theta_i = \theta_p$  then there is no reflection at the boundary, all energy travels in second medium  $n_2$

- (i) If  $\vec{E}$  oscillates not in the plane of page and  $\theta_i = \theta_p$  there would still be some reflection at the boundary!
- (ii) If that is the case, the direction of polarization (direction of oscillation of  $\vec{E}$ ) for the reflected rays (at  $\theta_i = \theta_p$ ) is  $\perp$  to plane of page  
 → Reason for  $\theta_i = \theta_p$  or polarizing angle (this angle "polarizes" the reflected rays)

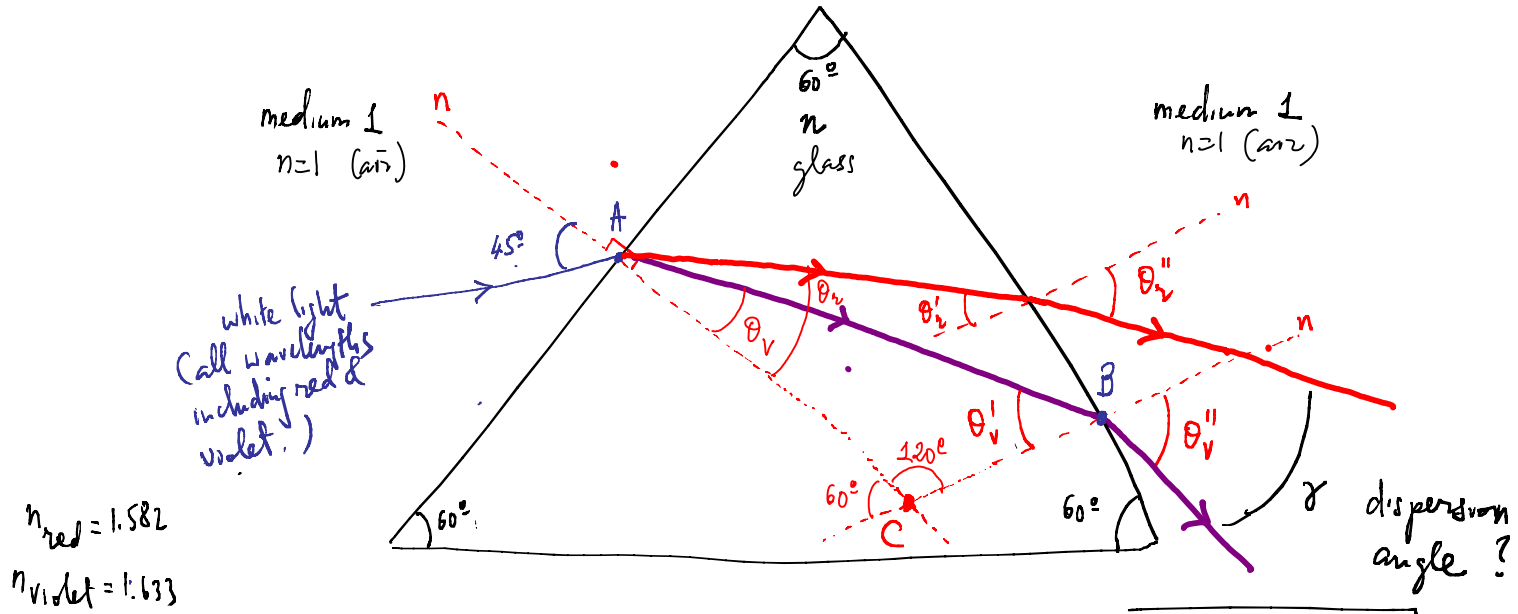
30.27

Prism spreads white light (incident beam  $\rightarrow$  outgoing cone)

disperses  $\rightarrow$  behaves differently for different wavelengths

$$\hookrightarrow \begin{cases} n_{red} = 1.582 = \frac{c}{v_{red}} \\ n_{violet} = 1.633 = \frac{c}{v_{violet}} \end{cases}$$

→ Determine dispersion angle  $\delta$



$n_{red} = 1.582$   
 $n_{violet} = 1.633$

$$\gamma = \theta''_v - \theta''_r ?$$

White light beam incident of left side of prism is spread out after refractions by prism  $\rightarrow$  determine dispersion angle  $\gamma$ .

Geometry: triangle ABC where C is intersection of normals to left & right sides

$\rightarrow$  Violet ray:  $\begin{cases} \theta_i = 45^\circ \\ \text{Refracted angle after hitting left boundary is } \theta_v \\ \text{Incident angle on right boundary is } \theta'_v \\ \text{Refracted angle after right boundary is } \theta''_v \end{cases}$

$$\theta_v + \theta'_v + 120^\circ = 180^\circ \text{ or } \theta'_v = 60^\circ - \theta_v$$

Law of Refraction or Snell's Law: (Violet rays)

(i) left boundary:  $1 \sin 45^\circ = n_v \sin \theta_v$   
 $\theta_v = \sin^{-1} \left( \frac{\sin 45^\circ}{n_v} \right)$   
 $\theta_v = \sin^{-1} \left( \frac{\frac{\sqrt{2}}{2}}{1.633} \right) = 25.5^\circ$

(ii) Right boundary: incident angle is  $\theta'_v = 60 - \theta_v = 34.5^\circ$   
 $n_v \sin 34.5^\circ = 1 \cdot \sin \theta''_v$   
 $\theta''_v = \sin^{-1} (n_v \sin 34.5^\circ) = \sin^{-1} (1.633 \cdot \sin 34.5^\circ)$   
 $\theta''_v = 67.7^\circ$

Similarly work out red rays:  $\Rightarrow$

(i) left boundary:  $1 \sin 45^\circ = n_r \sin \theta_r$   
 $\theta_r = \sin^{-1} \left( \frac{\frac{\sqrt{2}}{2}}{1.582} \right) = 26.5^\circ$

(ii) Right boundary: incident angle =  $\theta'_r = 60 - \theta_r = 33.5^\circ$

$$n_2 \sin 33.5^\circ = 1 \cdot \sin \theta_2''$$

$$\rightarrow \theta_2'' = \sin^{-1}(1.582 \cdot \sin 33.5^\circ)$$

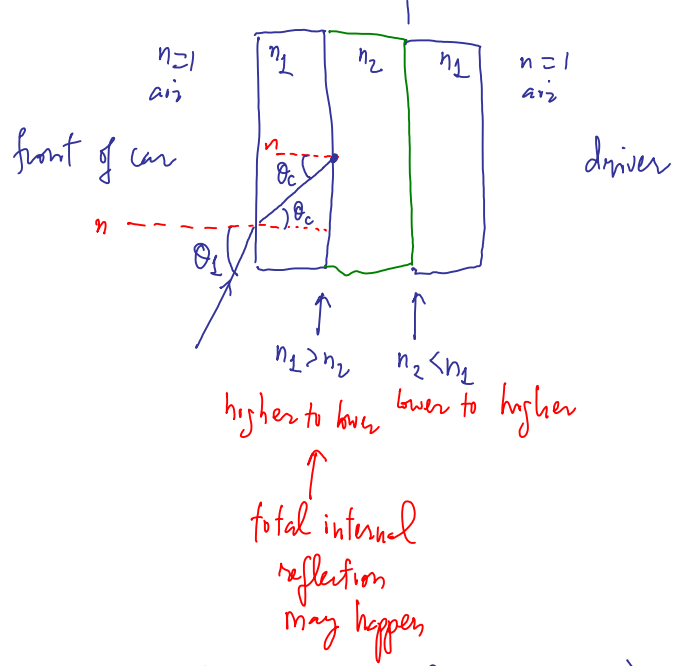
$$\theta_2'' = 60.7^\circ$$

$$\Rightarrow \gamma = \theta_1'' - \theta_2'' = 69.7^\circ - 60.7^\circ = 7^\circ$$

30.60

New materials for car windshields:

glass - plastic - glass  
 $n_1 = 1.55$     $n_2 = 1.48$     $n_3 = 1.55$



We want to calculate what incident angle  $\theta_1$  would refract into a ray that hits the 2nd boundary @ critical angle  $\theta_c$  which leads to total internal reflection (reduces visibility)

$$\theta_c = \sin^{-1}\left(\frac{n_2}{n_1}\right) = \sin^{-1}\left(\frac{1.48}{1.55}\right) = 73^\circ$$

→ At 1st boundary (air to glass):

$$1 \sin \theta_1 = 1.55 \sin \theta_c \rightarrow \theta_1 = \sin^{-1}(1.55 \sin 73^\circ)$$

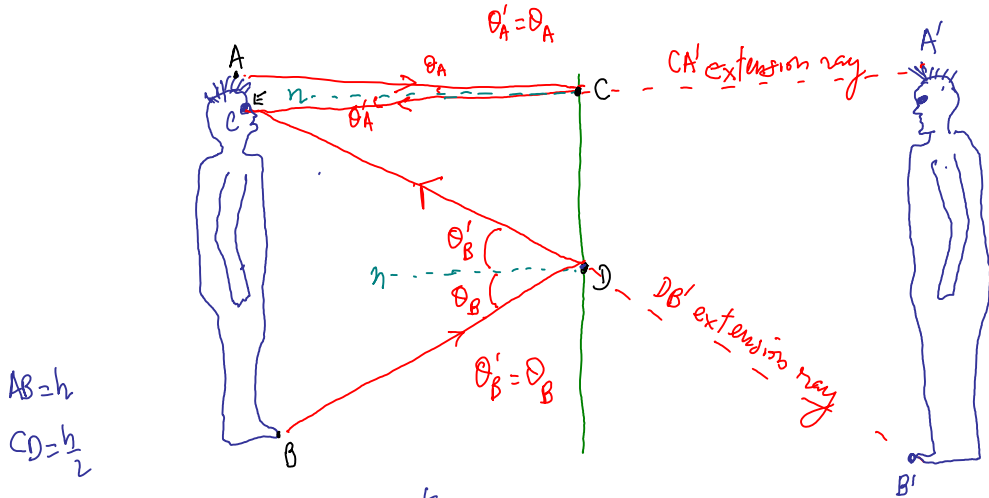
$$= \sin^{-1}(1.48)$$

Not possible!  
 → No problem w/ total internal reflection with this new windshield!

Form an image for a object through mirrors & lenses.

Mirrors:

(i) Mirror size so we can see our entire body in the mirror:



- a) Our eyes: we see two rays come in: 1) From C 2) From D
- b) We can't tell they originate at C or D

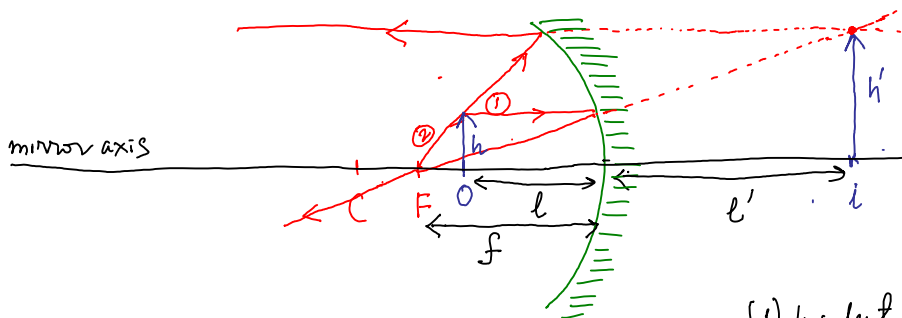
- c) Through mirrors our image is formed by extension rays
- d) Extension rays are virtual (only in our mind). There is no light @ A' & B'. Image by mirrors is virtual
- e) Mirror size:  $h, \frac{h}{2}, \frac{h}{3}$

Virtual image: { 1) Formed by extension rays  
2) No actual light rays converge at a virtual image

Real image: { 1) Formed by real light rays  
2) Actual light rays converge at real image

(ii) Curved mirrors:

Concave



mirrors & lenses:  
Standard notations:

- o: location of object
- i: location of image
- h: object height
- h': image height
- l: position of object
- l': position of image
- f: focal length



Curved mirror { F: focal point  
C: center of curvature

- 1) Incident ray || axis  $\rightarrow$  reflected ray passes thru F
- 2) Incident ray thru F  $\rightarrow$  reflected ray emerges || axis

Mirror equation :

$$\frac{1}{l} + \frac{1}{l'} = \frac{1}{f}$$

↳ Sign convention:

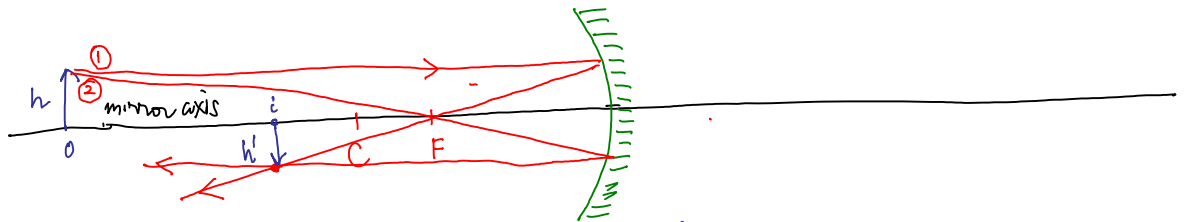
- $f$ 
  - + concave mirror 
  - convex mirror 

- $l'$ 
  - + if image is located same side of mirror as the object
  - if image is located the other side of mirror compared to object.

Magnification factor:  $M = \frac{h'}{h} = - \frac{l'}{l}$

↑  
geometry

iii) Can a curved mirror form a real image?



Real image, inverted { formed by real light rays which converge @ i

Lenses : { Thin  
Thick




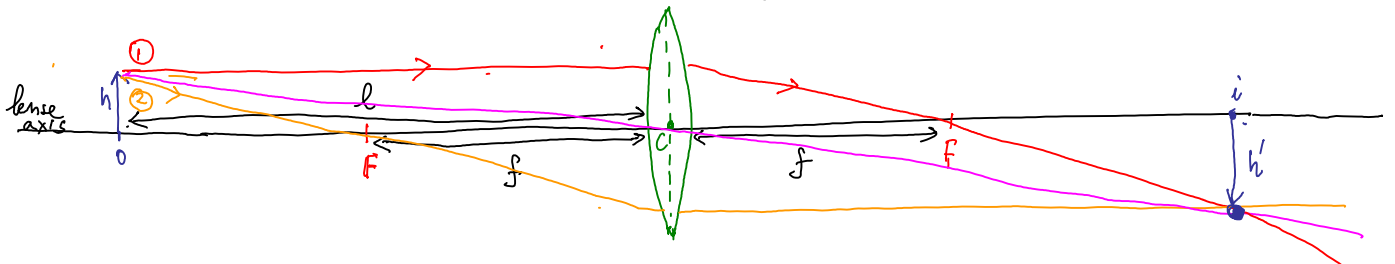
(i) Thin lenses :  → {  converging lens or convex lens  
 diverging lens or concave lens

Image formation for a thin converging lens:





Ray tracing

- ① Incident ray || axis emerges thru F the other side of lens
- ② Incident ray thru left F, emerges || axis the other side of lens
- ③ Incident ray thru center of lens C, keeps its direction.

↳ All three converge at top of image (inverted)

(Thin) Lens Equation:

$$\frac{1}{l} + \frac{1}{l'} = \frac{1}{f}$$

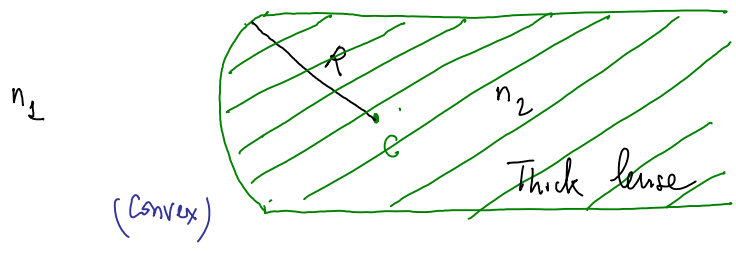
↳ Sign convention for lenses:

$f = \begin{cases} - & \text{concave or diverging lens} \\ + & \text{convex or converging lens} \end{cases}$   
 $l' = \begin{cases} + & \text{if image located other side of lens} \\ - & \text{if image located same side of lens} \end{cases}$

Magnification factor

$$M = \frac{h'}{h} = -\frac{l'}{l}$$

(ii) Thick lens #1

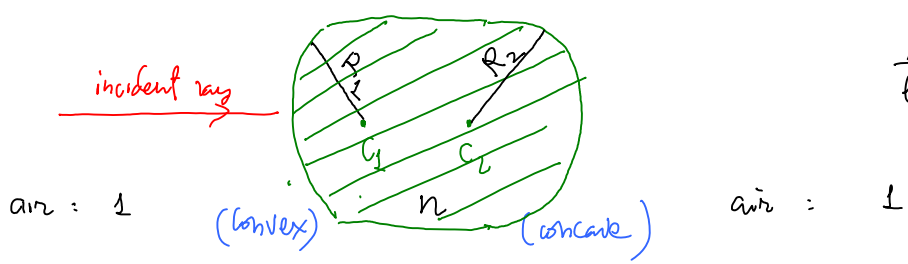


Thick lens #1 equation:

$$\frac{n_1}{l} + \frac{n_2}{l'} = \frac{n_2 - n_1}{R}$$

Sign convention:  
 $R = \begin{cases} + & \text{if convex} \\ - & \text{if concave} \end{cases}$   
 looking from incident side

(iii) Thick lens #2 (two curved boundaries)

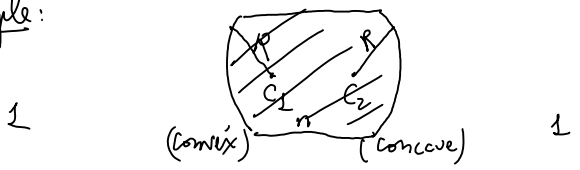


Thick lens #2 equation:

$$\frac{1}{l} + \frac{1}{l'} = \frac{1}{f} = (n-1) \left( \frac{1}{R_1} - \frac{1}{R_2} \right)$$

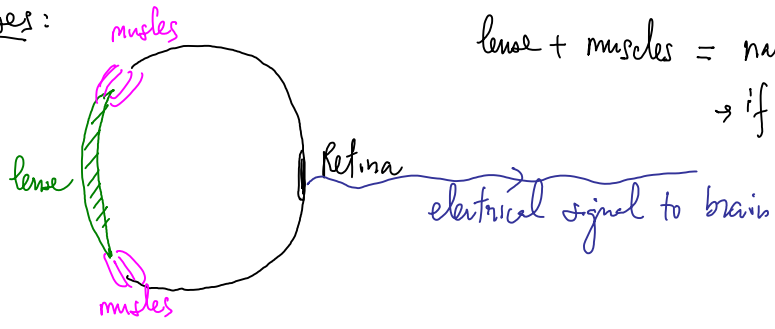
Signs:  $\begin{cases} R_1 + & \text{(convex)} \\ R_2 - & \text{(concave)} \end{cases}$

Example:



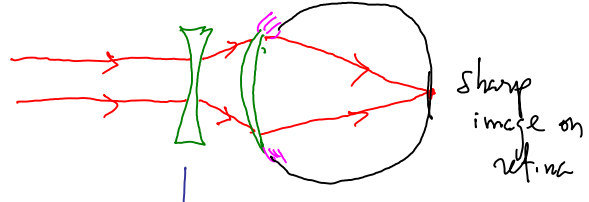
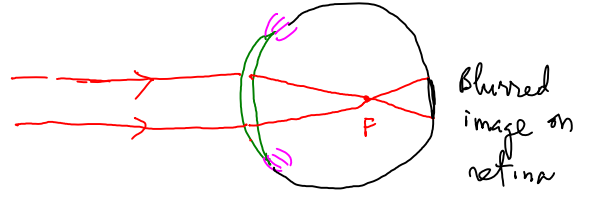
$$\Rightarrow \frac{1}{l} + \frac{1}{l'} = (n-1) \left( \frac{1}{R} - \frac{1}{\ominus R} \right) = (n-1) \frac{2}{R}$$

(iv) Eyes: lenses:



Near-sighted eye (myopic)

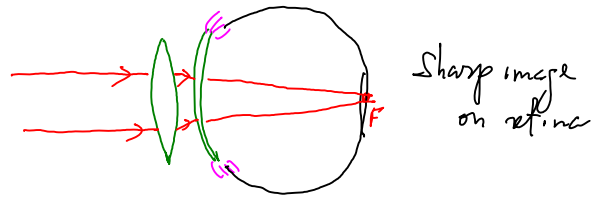
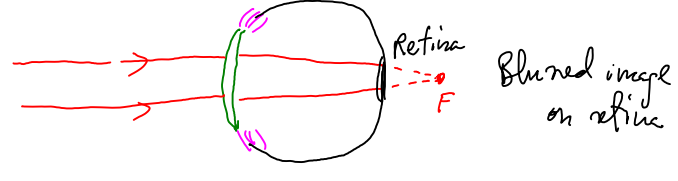
↓  
Focal point short of retina



↓  
 Diverging corrective lens ( $f$  negative)  
 Diopter =  $\frac{1}{f}$  ( $f$  in m)

Far-sighted eye (hyperopic)

Focal point beyond retina



Converging corrective lens ( $f$  +)  
 • Diopter =  $\frac{1}{f}$  ( $f$  in m)

Ch 32 Interference & Diffraction  
 (Physical Optics)

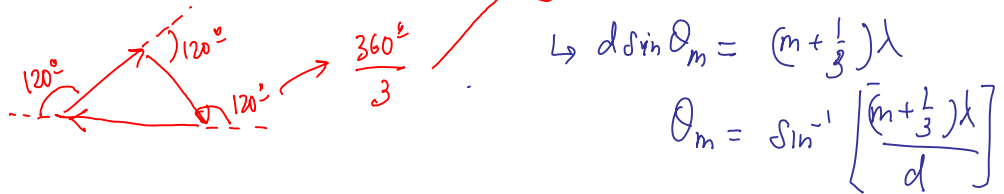
- (i) When light rays travel through small openings : no longer straight rays
- (ii) Superposition of light waves similar to that of sound waves or water waves (mechanical waves) in Physics I
  - ↳ 1) Double-slit
  - 2) Triple-slit
  - 3) Diffraction
  - 4) Thin film interference

Double-slit Interference:



(iv) C: dark spot  $\leftrightarrow$  destructive interference:

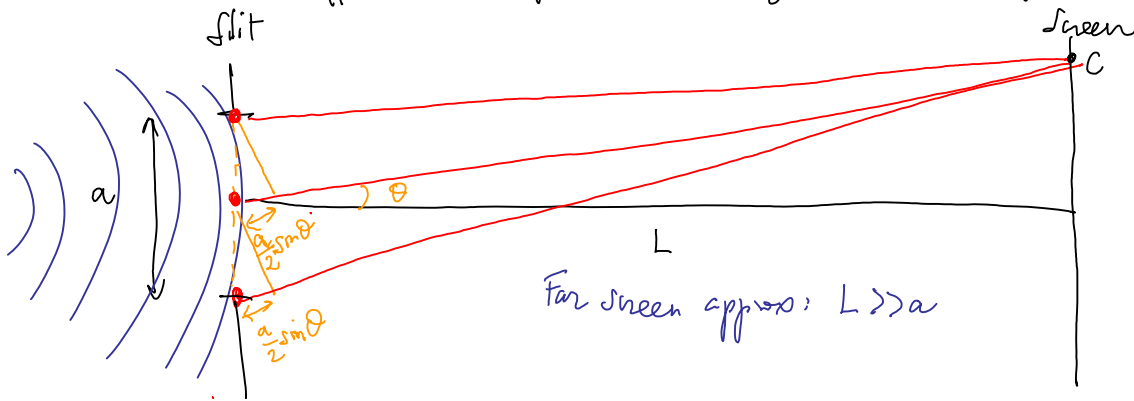
$\hookrightarrow$  3 waves  $\rightarrow$  out of phase by  $\frac{\lambda}{3}, \frac{4\lambda}{3}, \frac{7\lambda}{3}, \text{etc.}$



$\Rightarrow$  Generalize for  $N$  slits! :  $d \sin \theta_m = (m + \frac{1}{N}) \lambda = (Nm + 1) \frac{\lambda}{N}$

Diffraction: Superposition of waves out of a same slit: each point in a slit is the source of a baby wave.

$\hookrightarrow$  Single-slit diffraction  $\rightarrow$  pattern of bright & dark spots on a screen



(i) EM wave to slit  $\rightarrow$  Huygens principle  $\rightarrow$   $\infty$  number of baby waves in slit.

(ii) Far screen approx.  $L \gg a \rightarrow$   $\Delta \text{path} = \begin{cases} \frac{a}{2} \sin \theta & (1 \& 2 \text{ or } 2 \& 3) \\ a \sin \theta & (1 \& 3) \end{cases}$  } looking @ only 3 sources

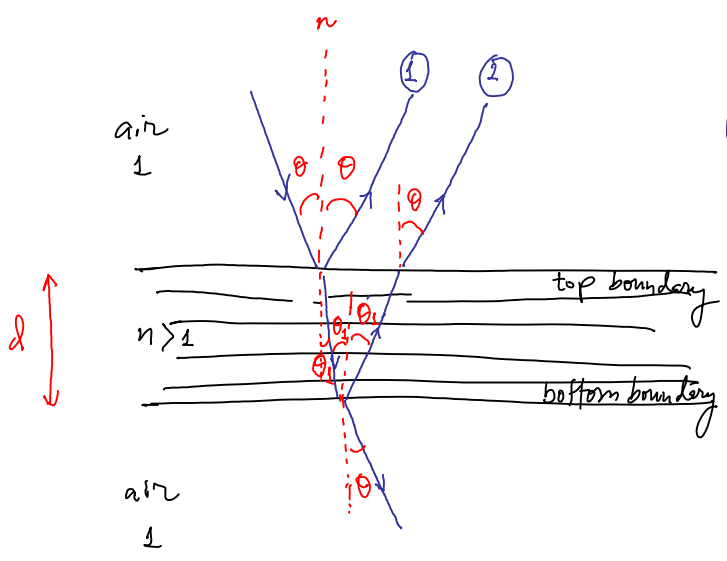
(iii) Dark spots :  $\Delta \text{path} = (2n+1) \frac{\lambda}{2}$   
 $\frac{a}{2} \sin \theta \rightarrow a \sin \theta = (2n+1) \lambda = \lambda, 3\lambda, 5\lambda, \text{etc.}$   
 $a \sin \theta \rightarrow a \sin \theta = (2n+1) \frac{\lambda}{2} = \frac{\lambda}{2}, \frac{3\lambda}{2}, \frac{5\lambda}{2}, \text{etc.}$

looking @ all sources in slit  $\rightarrow$   $a \sin \theta = n \lambda \quad (n=1, 2, 3, \text{etc.})$   
 dark spot in single-slit diffraction. ( $n \neq 0$ )

Diffraction limit: (optical instrument resolution) :  $\theta_{\min} = \frac{1.22 \lambda}{D} \leftarrow$  diameter of lens.

Thin film interference : geometrical + physical optics

Light incident on a thin film :



Rays 1 & 2 are parallel

- ① Reflected ray off top boundary of thin film  
 Since it reflects off a higher index medium  
 → wave is inverted → acquires an extra phase of  $\pi$  or  $\Delta path = \frac{\lambda}{2}$
- ② Comes from a reflection off bottom boundary or it reflects off a lower index medium  
 → wave is not inverted.  
 By travelling top-bottom-top this ray acquired  $\Delta path = 2d$  (thin film)

Superposition of waves 1 & 2 :

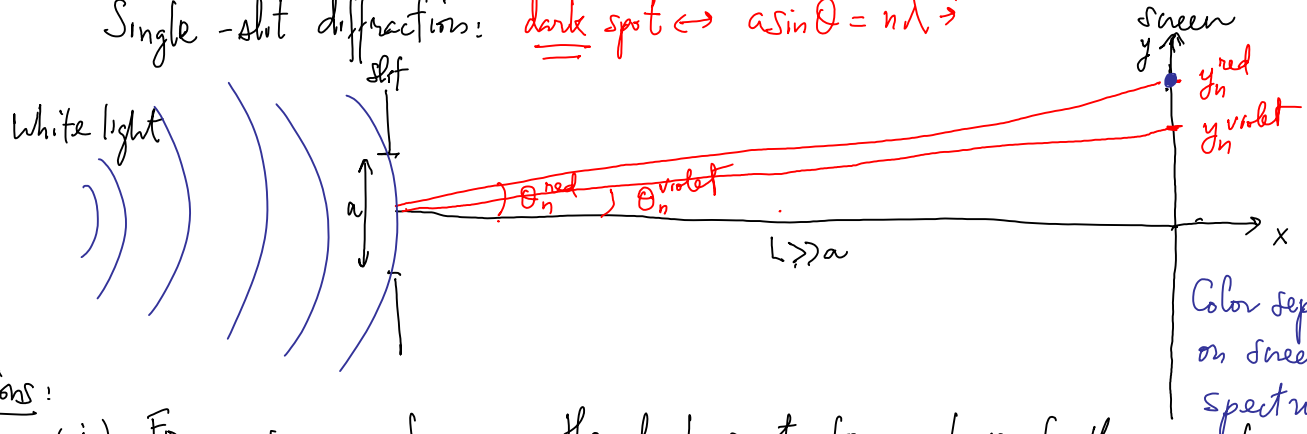
- ↳ Constructive interference : (bright rings)  
 $\Delta path_{12} = 2d - \frac{\lambda}{2} = n\lambda \quad (n=0,1,2, \dots)$   
 $\hookrightarrow 2d = n\lambda + \frac{\lambda}{2} = (n + \frac{1}{2})\lambda = \frac{(2n+1)\lambda}{2}$   
 $n=0,1,2, \dots$
- ↳ Destructive interference : (dark rings)  
 $\Delta path_{12} = 2d - \frac{\lambda}{2} = (2n+1)\frac{\lambda}{2} \quad (n=0,1,2, \dots)$   
 $\hookrightarrow 2d = (2n+1)\frac{\lambda}{2} + \frac{\lambda}{2} = 2n\frac{\lambda}{2} + \lambda$   
 $2d = (n+1)\lambda \quad (n=0,1,2, \dots)$

32.41

Visible light Spectrum  $\left\{ \begin{array}{l} \lambda_v = 400 \text{ nm} \\ \lambda_r = 700 \text{ nm} \end{array} \right.$

$\theta_n^{\text{red}} = \sin^{-1}\left(\frac{n\lambda_{\text{red}}}{a}\right)$   
 $\theta_n^{\text{violet}} = \sin^{-1}\left(\frac{n\lambda_{\text{violet}}}{a}\right) < \theta_n^{\text{red}}$

Single-slit diffraction: dark spot  $\leftrightarrow a \sin \theta = n\lambda$



Conclusions:

- (i) For a same order n, the dark spot for red is further up from center of screen than that for violet  $\theta_n^{\text{red}} > \theta_n^{\text{violet}}$
- (ii) A red dark spot of order n may overlap with the next violet dark spot of order n+1

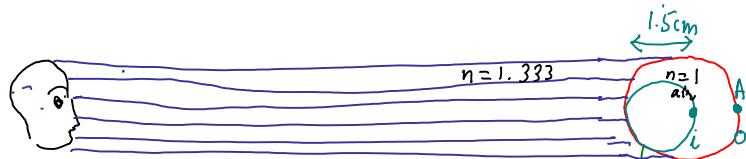
$$\sin \theta_n^{\text{red}} = \sin \theta_{n+1}^{\text{violet}}$$
$$\frac{n\lambda_{\text{red}}}{a} = \frac{(n+1)\lambda_{\text{violet}}}{a}$$
$$n\lambda_{\text{red}} = n\lambda_{\text{violet}} + \lambda_{\text{violet}}$$

$$n = \frac{\lambda_{\text{violet}}}{\lambda_{\text{red}} - \lambda_{\text{violet}}} = \frac{400 \text{ nm}}{700 \text{ nm} - 400 \text{ nm}} = \frac{4}{3} = 1.33$$

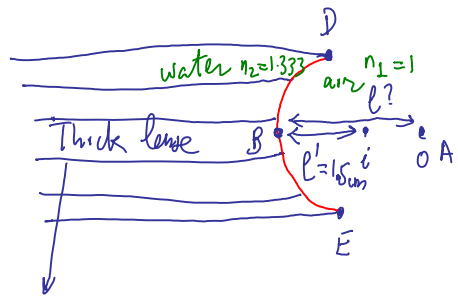
→ Any order above 1.33 or 2 or higher will have some overlap (dark red and next dark violet)  
→ Only order 1 (1st in spectrum) has no overlaps!

31.32

Spherical air bubble under water (through a thick lens made of water) appears to have  $d = 1.5 \text{ cm}$  → Actual diameter of air bubble?



Curved boundary of thick lens



$$\frac{n_1}{l} + \frac{n_2}{l'} = \frac{n_2 - n_1}{R}$$

↓

$$\frac{1}{2R} + \frac{1.333}{-1.5 \text{ cm}} = \frac{1.333 - 1}{-R}$$

$$= \frac{0.333}{-R} = \frac{0.666}{-2R} \rightarrow \frac{1.666}{2R} = \frac{1.333}{1.5} \rightarrow 2R = \frac{1.666 \cdot 1.5}{1.333}$$

(i) image of A through concave lens DBE position is  $l' = -1.5 \text{ cm}$  → bubble appears to have a diameter of 1.5 cm

Sign convention: a)  $l'$  is negative due to sign convention for lenses: image is on same side of lens as object

b) Light incident from the right → lens DBE is concave thick lens

$R$  is negative

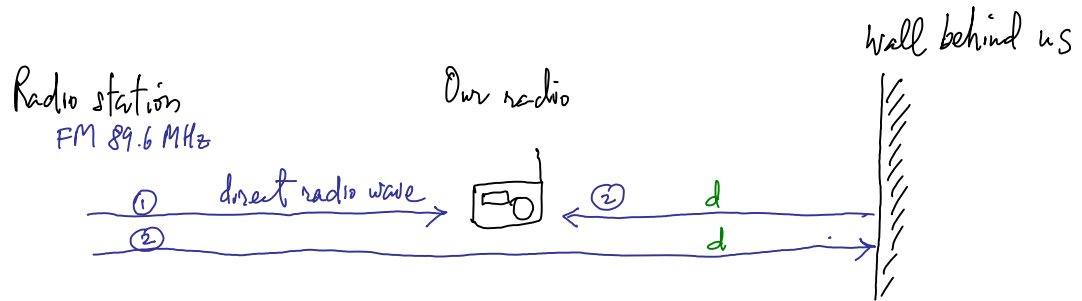
(ii) Light incident from air to water

$$n_1 = 1 \text{ (air)} ; n_2 = 1.333 \text{ (water)}$$

(iii) location of object is actual diameter of bubble:  $l = 2R$  (distance BA)

$$2R = 1.87 \text{ cm}$$

Actual diameter of bubble



① Direct wave from radio station

② Reflected wave off wall (extra phase of  $\pi$  or extra path  $\frac{\lambda}{2}$ ) with extra path of  $2d$

$$\Delta \text{path}_{12} = 2d - \frac{\lambda}{2}$$

→ Dead spot (destructive interference) at current location of our radio:

$$\Delta \text{path}_{12} = 2d - \frac{\lambda}{2} = (2m+1) \frac{\lambda}{2} \quad (m=0,1,2,3, \text{etc.})$$

$$\hookrightarrow d = \frac{1}{2} \left[ (2m+1) \frac{\lambda}{2} + \frac{\lambda}{2} \right] = \frac{1}{2} [m\lambda + \lambda]$$

$$\boxed{d_{\text{dead}} = (m+1) \frac{\lambda}{2}}$$

→ Clear spot (constructive interference)

$$\Delta \text{path}_{12} = 2d - \frac{\lambda}{2} = m\lambda \quad (m=0,1,2,3, \text{etc.})$$

$$\boxed{d_{\text{clear}} = \frac{1}{2} \left( m\lambda + \frac{\lambda}{2} \right) = \left( m + \frac{1}{2} \right) \frac{\lambda}{2}}$$

Current dead spot  $\rightarrow m$   $\rightarrow$  next clear spot  $\rightarrow m+1$ : what is the distance to move?

$$d_{\text{clear}(m+1)} - d_{\text{dead}(m)} = \left( m+1 + \frac{1}{2} \right) \frac{\lambda}{2} - (m+1) \frac{\lambda}{2} = \frac{\lambda}{4} = \frac{3.352}{4} = 0.838 \text{ m}$$

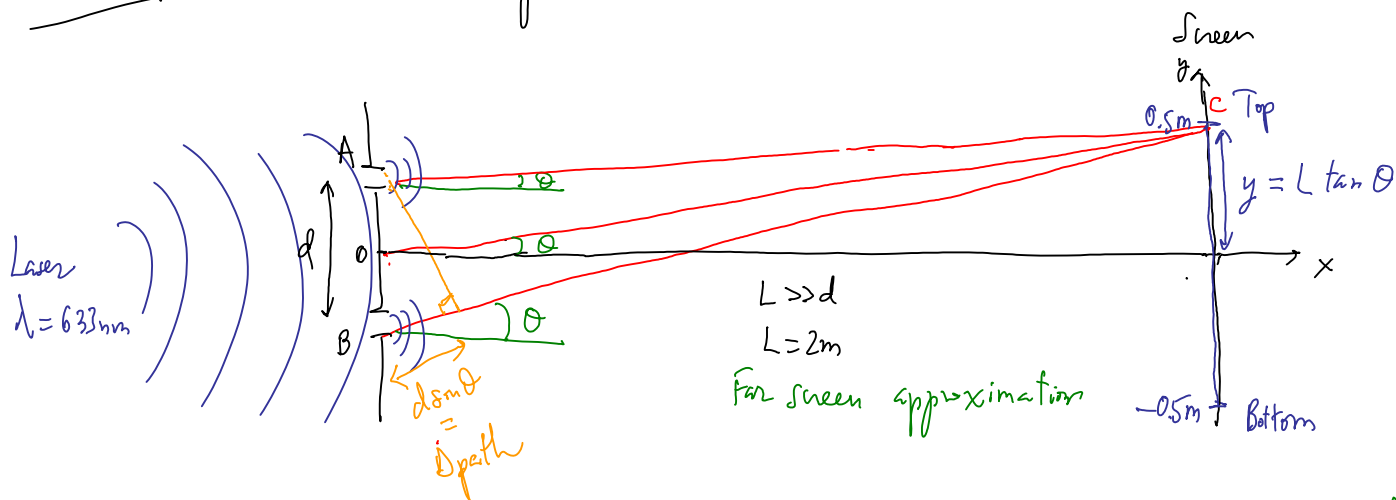
$$f = 89.5 \cdot 10^6 \text{ Hz} \rightarrow c = \lambda \cdot f \rightarrow \lambda = \frac{c}{f}$$

$$\lambda = \frac{3 \cdot 10^8}{89.5 \cdot 10^6} = 3.352 \text{ m}$$



32.37

### Two-slit interference:



Highest order bright fringe that fits on screen?

$m_{max}$ ?

constructive interference

$y = 0.5\text{ m}$  (top of screen)

$d = 0.1\text{ mm} = 10^{-4}\text{ m}$   
 $d = 10\text{ }\mu\text{m} = 10^{-5}\text{ m}$

$$d \sin \theta = m \lambda \quad (m = 0, 1, 2, 3 \text{ etc...})$$

$$d \sin \theta = m \lambda \rightarrow \theta = \sin^{-1} \left( \frac{m \lambda}{d} \right)$$

$$y = L \tan \theta = L \tan \left( \sin^{-1} \left( \frac{m \lambda}{d} \right) \right)$$

$$0.5 = 2 \tan \left( \sin^{-1} \left( m_{max} \cdot \frac{633 \cdot 10^{-9}}{d} \right) \right)$$

(i)  $d = 10^{-4}\text{ m} \rightarrow \tan^{-1} 0.25 = \sin^{-1} \left( m_{max} \frac{633 \cdot 10^{-9}}{10^{-4}} \right)$

$$m_{max} = \frac{\sin \left( \tan^{-1} 0.25 \right)}{633 \cdot 10^{-5}} = 38.22$$

orders in whole numbers  $\rightarrow m_{max} = 38$

(ii)  $d = 10^{-5}\text{ m} \rightarrow$

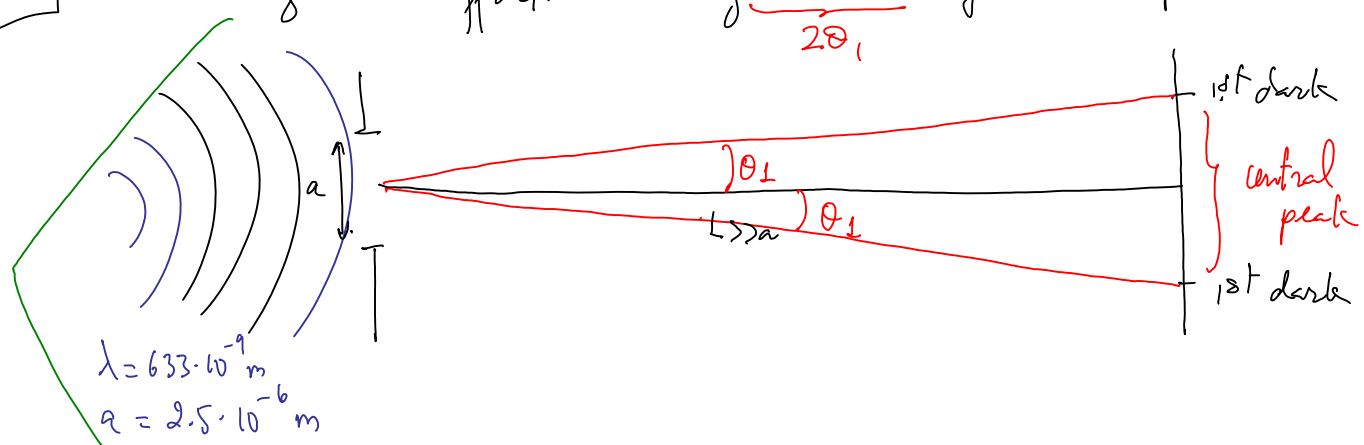
$$m_{max} = \frac{\sin \left( \tan^{-1} 0.25 \right)}{633 \cdot 10^{-4}} = 3.822$$

$m_{max} = 3$

reason: smaller slit spacing fringes are further apart  $\rightarrow$  only 3 will fit.

32.27

Single-slit diffraction: angular width of central peak.



$\lambda = 633 \cdot 10^{-9} \text{ m}$   
 $a = 2.5 \cdot 10^{-6} \text{ m}$

Dark spots:  $a \sin \theta = n \lambda$  ( $n = 1, 2, 3, \dots$ )

1st dark spot,  $\theta_1 = \sin^{-1} \left( \frac{\lambda}{a} \right) = \sin^{-1} \left( \frac{633 \cdot 10^{-9}}{2.5 \cdot 10^{-6}} \right) = 14.7^\circ$

$2\theta_1 = 29.4^\circ$

31.42

- (i) Concave mirror ( $f$  negative)
- (ii) Virtual image (the other side of mirror) ( $l'$  negative)
- (iii)  $M = \frac{h'}{h} = -\frac{l'}{l} = 1.8$  (positive  $\rightarrow$  image is upright!)  $\Rightarrow l' = -1.8l$
- (iv)  $l = 22 \text{ cm}$

$\rightarrow$  Calculate radius of curvature  $R$  for concave mirror: from focal length:  
 $|f| = \frac{R}{2}$

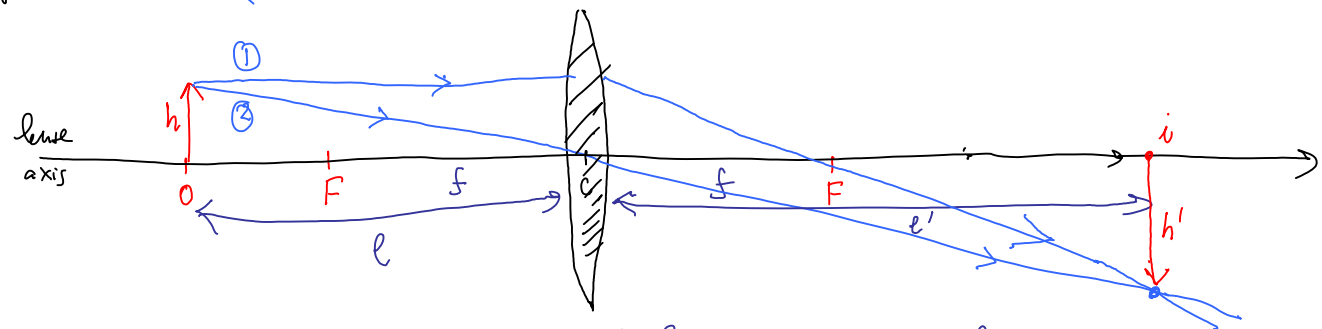
focal length  $f$ : from mirror equation:

$\frac{1}{l} + \frac{1}{l'} = \frac{1}{f} \rightarrow f = \left( \frac{1}{22 \text{ cm}} + \frac{1}{-1.8 \cdot 22} \right)^{-1} = \left[ \frac{1}{22} \left( 1 - \frac{1}{1.8} \right) \right]^{-1}$   
 $f = 49.4 \text{ cm} \rightarrow R = 98.8 \text{ cm}$

31.50

Calculate position of image through a converging lens - or convex lens  $\rightarrow f$  is positive:  $f = +35 \text{ cm}$

a)  $l = 60 \text{ cm}$



$l'$  positive: image the other side of lens  $\rightarrow$  sep b/w o & i is  $l + l'$

lense equation:  $\frac{1}{l} + \frac{1}{l'} = \frac{1}{f} \rightarrow \frac{1}{l'} = \frac{1}{f} - \frac{1}{l} = \frac{l-f}{lf} \rightarrow l' = \frac{lf}{l-f}$

$l' = \frac{40 \cdot 35}{40-35} = 280 \text{ cm} \rightarrow \text{sep. o \& i is } l+l' = 40+280 = 320 \text{ cm}$

b)  $l = 30 \text{ cm}$

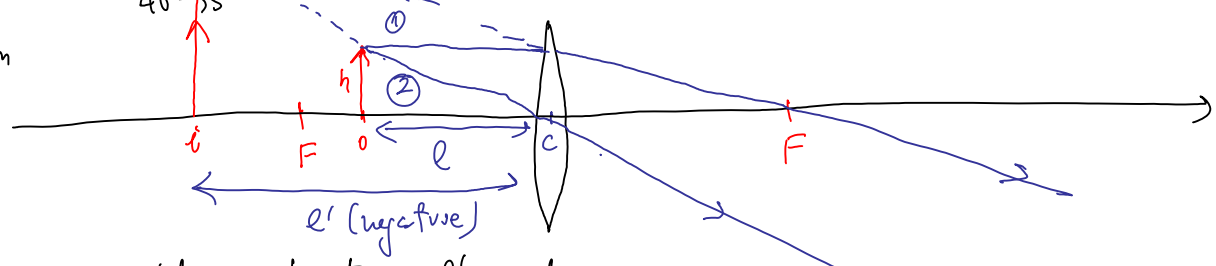


image is same side as object  $\rightarrow l'$  negative  
 image is formed by extension rays  $\rightarrow$  virtual & upright

$l' = \frac{30 \cdot 35}{30-35} = -210 \text{ cm} \rightarrow \text{sep. b/w o \& i } |30 - 210| = 180 \text{ cm}$



Ch 27

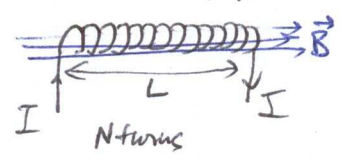
Faradays' Law : 1) time-varying magnetic flux induces a voltage along a closed loop where the flux goes through, that opposes the change of magnetic flux:  

$$\mathcal{E} = - \frac{d\Phi_B}{dt}$$

2) w/o a wire the induced voltage or electric field is there. If there is a wire on that loop, the induced  $\vec{E}$  drives a current in that wire

Inductance { self  $L = \frac{\Phi}{I}$  (one solenoid)  
 mutual  $M = \frac{\Phi_2}{I_1}$  (two solenoids)

solenoid of {  $N$  turns  
 length  $L$   
 $I$  in each turn } creates  $B = \mu_0 \frac{N}{L} I$   
 $n$ : # turns per unit length.



Energy { electric:  $U_E = \frac{1}{2} CV^2$  ←  $C$  inerts to change in voltage  
 $u_E = \frac{1}{2} \epsilon_0 E^2$   
 magnetic:  $U_M = \frac{1}{2} LI^2$  ←  $L$  inerts to change in current  
 $u_M = \frac{1}{2\mu_0} B^2$

Ch 29

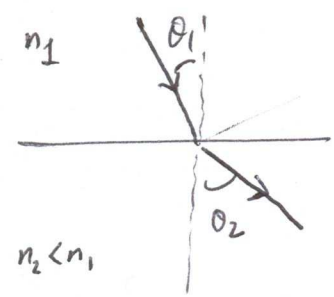
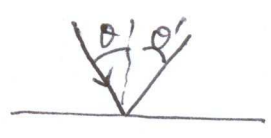
Maxwell's equation: { 1) Displacement current  $\mu_0 \epsilon_0 \int \frac{\partial \vec{E}}{\partial t} \cdot d\vec{A}$   
 allows complete symmetry b/w equations relating  $\vec{E}$  &  $\vec{B}$  in vacuum:  $v = \frac{\omega}{k} = \sqrt{\frac{1}{\mu_0 \epsilon_0}}$   
 Ampere's & Faraday's law  
 $E(t) \rightarrow B(t) \rightarrow E(t) \dots \rightarrow$  propagates in vacuum!  
 2) Vector nature of  $\vec{E}$  &  $\vec{B} \rightarrow$  polarization  
 Intensity  $S \propto E^2$

Radiation pressure:  $\frac{S}{c}$   
 (pressure comes from transfer of momentum to the reflecting surface)

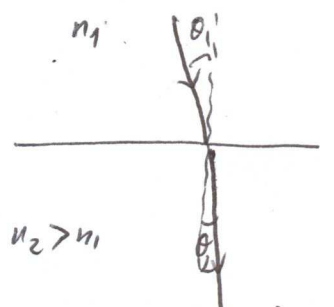
ch 30

Reflection & Refraction

- Law of reflection  $\theta' = \theta$
- Law of refraction or Snell's Law:  $n_1 \sin \theta_1 = n_2 \sin \theta_2$



wave front is rotated CCW



- > wave front rotated CW
- > if  $\theta_1 \geq \theta_c = \sin^{-1}(\frac{n_2}{n_1})$
- > Total internal reflection

- Brewster's angle:  $\vec{E}$  in plane of page &  $\theta = \theta_B$  or  $\theta_p = \tan^{-1}(\frac{n_2}{n_1})$
- > No reflection, all refraction.

- Multiple mirrors -> use triangular geometry to relate outgoing ray direction to incident ray direction
- Dispersion occurs when the index of refraction  $n$  varies for different wavelengths that come in the incident light.

ch 31

Lenses & Mirrors

Mirror equation  $= \frac{1}{l} + \frac{1}{l'} = \frac{1}{f}$

$M = \frac{h'}{h} = -\frac{l'}{l}$

$f$	+ concave
	- convex
$l'$	+ i same side as o
	- i other side as o

Lenses Thin:  $\frac{1}{l} + \frac{1}{l'} = \frac{1}{f}$

$f$	+ concave or diverging lenses
	+ convex or converging lenses
$l'$	+ i opposite side as o
	- i same side as o

Thick 1 boundary:  $\frac{n_1}{l} + \frac{n_2}{l'} = \frac{n_2 - n_1}{R}$   $R$  + convex / - concave

Thick 2 boundaries:  $\frac{1}{f} = (n-1)(\frac{1}{R_1} - \frac{1}{R_2})$   $R$  + convex / - concave

From incident side

Ch 32

Interference & Diffraction

Interference

spacing b/w slits is  $d$

two-slit

Bright spot  $\Delta path = d \sin \theta = m \lambda$  ( $m = 0, 1, 2, 3, \text{etc.}$ )  
 $\theta_m = \sin^{-1} \left( \frac{m \lambda}{d} \right)$ ;  $y_m = L \tan \theta_m$

Dark spot  $\Delta path = d \sin \theta = (2m+1) \frac{\lambda}{2}$  ( $m = 0, 1, 2, 3, \text{etc.}$ )  
 $\theta_m = \sin^{-1} \left( \frac{(2m+1) \lambda}{2d} \right)$ ;  $y_m = L \tan \theta_m$

three-slit

Bright spot:  $\Delta path = d \sin \theta = m \lambda$

Dark spot:  $\Delta path = d \sin \theta = (m + \frac{1}{3}) \lambda$  ( $m = 0, 1, 2, 3, \text{etc.}$ )  
 $\theta_m = \sin^{-1} \left[ \frac{(m + \frac{1}{3}) \lambda}{d} \right]$ ;  $y_m = L \tan \theta_m$

thin film  
↓ thickness  
is  $d$   
and index is  $n$

constructive:  $2d = (2n+1) \frac{\lambda}{2}$  ( $n = 0, 1, 2, 3, \text{etc.}$ )

destructive:  $2d = n \lambda$  ( $n = 0, 1, 2, 3, \text{etc.}$ )

This  $\lambda$  wavelength on the film  $\lambda = \frac{\lambda_0}{n}$

Diffraction: dark spots:  $a \sin \theta = n \lambda$  ( $n = 1, 2, 3, \text{etc.}$ )

↳ single slit of width  $a$ .

↳ overlap of ~~order~~ dark spots for red & violet of consecutive order

↳ Optical instrument resolution:  $\theta_{min} = \frac{1.22 \lambda}{D}$ ;  $D$ : diameter of lens or slit