

16.76

(16.3):  $\Delta Q = mc\Delta T$   $\xrightarrow{\quad\quad\quad} \frac{\Delta Q}{\Delta t} = mc \frac{\Delta T}{\Delta t} \xrightarrow[\lim_{\Delta t \rightarrow 0}]{} \frac{dQ}{dt} = mc \frac{dT}{dt}$

(16.5):  $H = -kA \frac{\Delta T}{\Delta x} = \frac{dQ}{dt}$  (Heat loss rate)

$\Rightarrow mc \frac{dT}{dt} = -kA \frac{\Delta T}{\Delta x} \Rightarrow \frac{dT}{dt} = \frac{-kA}{mc\Delta x} \Delta T \Rightarrow \boxed{\frac{dT}{dt} \propto \Delta T}$

constants

**Newton's Law of cooling**  
 (Rate of change of temperature is proportional to the temperature difference between the house and its surroundings)

$$\frac{dT}{dt} = -\frac{1}{mc} \cdot \frac{kA}{\Delta x} \cdot \Delta T = -\frac{1}{C} \cdot \frac{1}{R} \cdot \Delta T = -\frac{35}{6.5 \cdot 10^6 \cdot 6.67 \cdot 10^{-3}} = -8.07 \cdot 10^{-4} \frac{^\circ K}{s}$$

- Heat capacity  $C \equiv mc = 6.5 \cdot 10^6 \frac{J}{^\circ K}$
- Thermal resistance:  $R \equiv \frac{\Delta x}{kA} = 6.67 \cdot 10^{-3} \frac{^\circ K}{W}$
- Temperature difference:  $\Delta T = 20^\circ C - (-15^\circ C) = 35^\circ K$

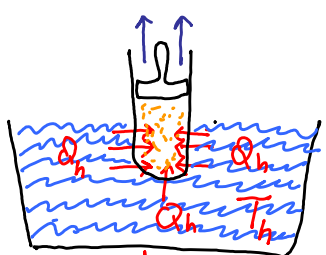
How long would it take to go from  $20^\circ C$  to  $0^\circ C$  freezing point:  $(\frac{dT}{dt} = 8.07 \cdot 10^{-4} \frac{^\circ K}{s})$

$$t = \frac{\Delta T}{\frac{dT}{dt}} = \frac{20^\circ K}{8.07 \cdot 10^{-4} \frac{^\circ K}{s}} = 247740 s \cdot \frac{1h}{3600s} = 6.88 \text{ hrs.}$$

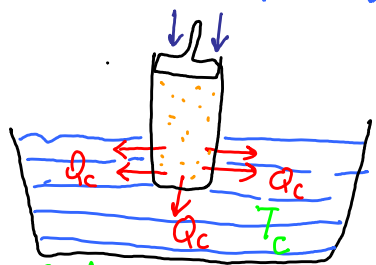
## Ch 19 2nd Law of Thermodynamics

- ↳ Heat engine
- ↳ Heat reservoir: source of heat that stays at constant temperature

Heat engine: placing an ideal gas in a cylinder + piston in thermal contact with a hot heat reservoir @  $T_h$ , then in thermal contact with a cold heat reservoir @  $T_c$ , then repeating this cycle.



**Hot heat reservoir**  
 As heat transfers in, gas KE is increased, its temperature & pressure are increased → gas expands, piston is pushed up, work done by gas  $W$  is positive.

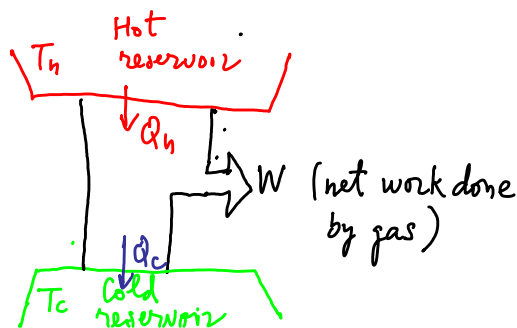


**Cold heat reservoir**  
 To prepare gas for further work on piston, it is brought in thermal contact with a cold reservoir. As heat transfers out gas KE is decreased, so are its temperature & pressure → gas compresses, piston comes back down,

This continues until the gas reaches T.D equilibrium with hot reservoir @  $T_h$

work done by gas is negative. This continues until the gas reaches T.D equilibrium with cold reservoir @  $T_c$  (28)

### Heat engine diagram:



### Efficiency of Heat Engine:

1) 1st Law of T.D:  $\Delta U_{\text{Heat engine}} = Q - W$  (Heat absorbed minus work done by gas)  
 $= Q_h - Q_c - W$

2) Heat reservoirs are at constant temperature  $\rightarrow$  heat transfers in/out of Heat engine under isothermal processes  $\rightarrow$  ideal gas

$\Delta T = 0 \Rightarrow \Delta U_{\text{Heat engine}} = 0$

$\Rightarrow Q_h - Q_c - W = 0 \quad \text{or} \quad \boxed{Q_h - Q_c = W}$

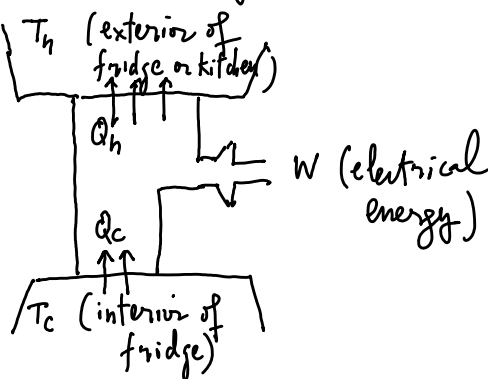
3) Efficiency of a heat engine using ideal gas:

$$e \equiv \frac{W}{Q_h} = \frac{Q_h - Q_c}{Q_h} = 1 - \frac{Q_c}{Q_h} \Rightarrow e < 1 \quad e = 1 - \frac{|Q_c|}{|Q_h|}$$

$|Q_c| < |Q_h| \rightarrow \frac{|Q_c|}{|Q_h|} < 1 \rightarrow \boxed{e < 1} \rightarrow$  2nd Law of T.D: it is impossible

to build a heat engine working in cycles that extracts heat from a hot reservoir (and returning some of it to a cold reservoir) that can deliver 100% of work or  $e < 1$

### Reversed heat engine (refrigerators)



2<sup>nd</sup> Law of TD: it is impossible to transfer heat from a cold reservoir to a hot reservoir without requiring any work  $W$

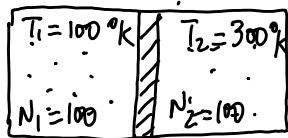
Coefficient of performance C.O.P.  $\equiv \frac{Q_c}{W}$

3<sup>rd</sup> Law TD:

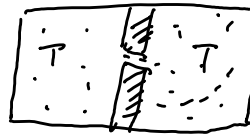
↳ Entropy:  $\Delta S \equiv \int_1^2 \frac{dQ}{T}$

- ↳ (i) Degree of disorder  
 (ii) The entropy of a closed system (no external assistance) can never decrease or  $\Delta S \geq 0$

Example: two gases at different temperatures once they are mixed up they would never separate back to their original temperatures (without external assistance)



→

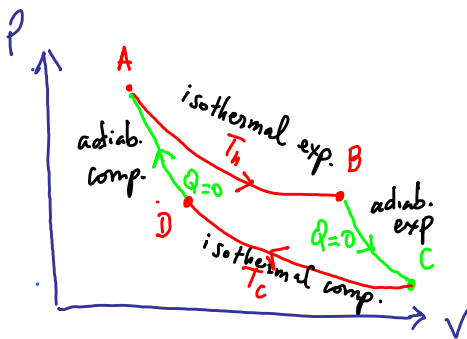


Hotter molecules tend to go left, some of cold molecules get pushed to the right, they will arrive at same final temperature  $T$ . This mix  $\sim$  higher level of disorder ( $\Delta S > 0$ )

Heat engines { Carnot engines: max efficiency  $e_{max} = 1 - \frac{T_c}{T_h}$  (will derive)  
 Otto Cycle engines:  $e < e_{max}$

Carnot Engines: (i) a type of heat engine, follos 4 reversible processes (two isothermal, two adiabatic)

(ii)  $e_{Carnot} = e_{max} = 1 - \frac{T_c}{T_h}$



$Q_h$ : heat absorbed from hot reservoir during isothermal expansion  $A \rightarrow B$

$Q_h = W = nRT_h \cdot \ln\left(\frac{V_B}{V_A}\right)$

$\Delta U = 0 = Q - W$  (isothermal)

$Q_c$ : heat ejected to cold reservoir during isothermal compression  $C \rightarrow D$

$Q_c = nRT_c \ln\left(\frac{V_D}{V_C}\right)$  (since  $V_D < V_C \rightarrow Q_c < 0$  heat loss to cold reservoir)

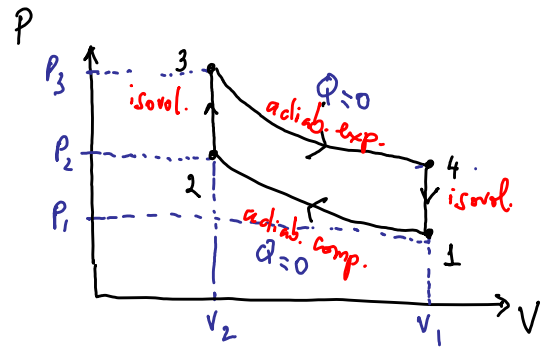
$B \rightarrow C$  : adiabatic expansion :  $T_B V_B^{\gamma-1} = T_C V_C^{\gamma-1} \Rightarrow \left(\frac{V_B}{V_C}\right)^{\gamma-1} = \frac{T_C}{T_B} = \frac{T_C}{T_h}$   
 $D \rightarrow A$  : adiabatic compression :  $T_D V_D^{\gamma-1} = T_A V_A^{\gamma-1} \Rightarrow \left(\frac{V_D}{V_A}\right)^{\gamma-1} = \frac{T_A}{T_D} = \frac{T_h}{T_c}$

$\left. \begin{aligned} \frac{V_B}{V_C} = \frac{V_A}{V_D} \\ \frac{V_B}{V_A} = \frac{V_C}{V_D} \end{aligned} \right\} \text{or } \frac{V_B}{V_A} = \frac{V_C}{V_D}$

$\eta_{\text{Carnot}} = \eta_{\text{max}} = 1 - \frac{|Q_c|}{|Q_h|} = 1 - \frac{|nRT_c \ln(\frac{V_D}{V_C})|}{|nRT_h \ln(\frac{V_B}{V_A})|} = 1 - \frac{T_c}{T_h} \left| \frac{\ln(\frac{V_D}{V_C})}{\ln(\frac{V_B}{V_A})} \right|$

$\left[ 1 - \frac{T_c}{T_h} \right]$

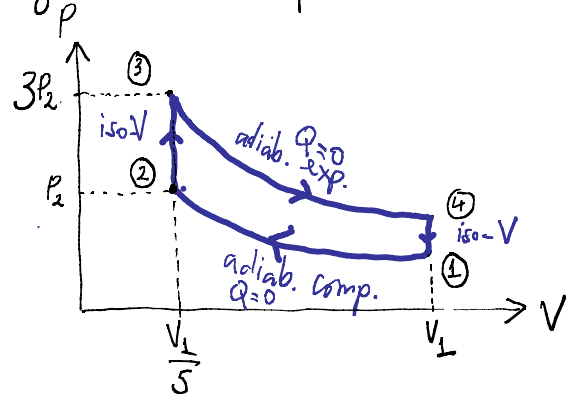
Otto Cycle Engine: (i) Another type of heat engine. It follows four reversible processes : 2 adiabatic, 2 isovolumic  
 (ii)  $\eta_{\text{otto}} < \eta_{\text{max}}$



Applications of reversible processes in Ch18 to the calculations of heat engine efficiencies

19.53] Given a gasoline engine operating in the Otto Cycle (2 adiabatic + 2 isovolumic processes) and given its PV diagram, find its efficiency  $e = \frac{W}{Q_h}$

Step 1: Diagram with information: PV diagram is given



$\gamma = \frac{C_p}{C_v}$  specific heat ratio

$e = \frac{W}{Q_h}$

Step 2: Relevant equations: eqs. for iso-V & adiabatic processes.

$e = \frac{W}{Q_h} = \frac{Q_h - Q_c}{Q_h} = 1 - \frac{|Q_c|}{|Q_h|} < 1$

Heat reservoirs @ constant T: iso-V ② → ③ ( $P_3 = 3P_2$ )

$\Delta U = 0 = Q_h - Q_c - W$

(i) Heat exchange during iso-volumic processes:  $c_v = \frac{1}{n} \frac{Q}{\Delta T} \Rightarrow Q = n c_v \Delta T$

$$\left\{ \begin{array}{l} Q_h = Q_{23} = n c_v (T_3 - T_2) \\ Q_c = Q_{41} = n c_v (T_1 - T_4) \end{array} \right\} \Rightarrow e = 1 - \frac{|T_1 - T_4|}{|T_3 - T_2|}$$

Now we need to relate these temperatures to  $\gamma$

↑ Adiabatic processes  $T V^{\gamma-1} = \text{constant}$

(ii)  $T \cdot V^{\gamma-1}$  is constant during adiabatic processes: ① → ② & ③ → ④

$$\left\{ \begin{array}{l} T_1 V_1^{\gamma-1} = T_2 V_2^{\gamma-1} \\ T_3 V_3^{\gamma-1} = T_4 V_4^{\gamma-1} \end{array} \right. \left\{ \begin{array}{l} \text{comes from } P_1 V_1^\gamma = P_2 V_2^\gamma \\ \& P_1 = \frac{nRT_1}{V_1}; P_2 = \frac{nRT_2}{V_2} \end{array} \right.$$

There are some information on the volumes:  $\left\{ \begin{array}{l} V_4 = V_1 \\ V_3 = V_2 = \text{given } \frac{V_1}{5} \end{array} \right.$

$$\left\{ \begin{array}{l} T_1 V_1^{\gamma-1} = T_2 \left(\frac{V_1}{5}\right)^{\gamma-1} \\ T_4 V_1^{\gamma-1} = T_3 \left(\frac{V_1}{5}\right)^{\gamma-1} \end{array} \right\} \Rightarrow \frac{T_1}{T_4} = \frac{T_2}{T_3}$$

$\frac{T_4}{T_3} = \frac{1}{5^{\gamma-1}} \Rightarrow T_3 = T_4 5^{\gamma-1}$

Rewrite equation for  $e$  with these results:

$$e_{\text{otto}} = 1 - \frac{|T_1 - T_4|}{|T_3 - T_2|} = 1 - \frac{\cancel{T_4} \left| \frac{T_1}{\cancel{T_4}} - 1 \right|}{T_3 \left| 1 - \frac{\cancel{T_2}}{T_3} \right|} = 1 - \frac{T_4}{T_3}$$

a)  $\boxed{e_{\text{otto}} = 1 - \frac{1}{5^{\gamma-1}} = 1 - 5^{1-\gamma}}$  ( $\frac{1}{a} = a^{-1}$ )

b) Write  $T_{\text{max}}$  (highest temperature in the Otto Cycle) in terms of  $T_{\text{min}}$  (min temp. in the cycle)

adiab. comp  $\left. \begin{matrix} T_1 \text{ lowest} \rightarrow T_{\text{min}} = T_1 \\ T_2 > T_1 \end{matrix} \right\}$  Write  $T_3$  in terms of  $T_1$

iso-V  $\left. \begin{matrix} (P_3 = 3P_2) \\ T_3 > T_2 \rightarrow T_{\text{max}} = T_3 \end{matrix} \right\}$

adiab. exp.  $\left. \begin{matrix} (V_4 = 5V_3) \\ T_4 < T_3 \\ P_4 > P_1 \rightarrow T_4 > T_1 \end{matrix} \right\}$

(i) Adiabatic  $3 \rightarrow 4$ :  $T_3 = T_4 5^{\gamma-1}$  (since  $V_3 = \frac{V_1}{5}$  &  $V_4 = V_1$ )

(ii) Adiabatic  $3 \rightarrow 4$  &  $1 \rightarrow 2$ :  $\frac{T_1}{T_4} = \frac{T_2}{T_3}$

(iii) Ideal gas equation:  $PV = nRT \rightarrow \frac{T_2}{T_3} = \frac{\frac{P_2 V_2}{nR}}{\frac{P_3 V_3}{nR}} = \frac{P_2}{P_3} \frac{V_2}{V_3} = \frac{P_2}{P_3} \cdot \frac{1}{3}$

$P_3 = 3P_2$  given  
↑ iso-V  $\Rightarrow V_2 = V_3$

$\Rightarrow \frac{T_1}{T_4} = \frac{T_2}{T_3} = \frac{1}{3} \Rightarrow \boxed{T_4 = 3T_1}$

$\Rightarrow T_3 = T_4 5^{\gamma-1} = 3T_1 \cdot 5^{\gamma-1} = 3 \cdot 5^{\gamma-1} T_1 \Rightarrow \boxed{T_{\text{max}} = 3 \cdot 5^{\gamma-1} \cdot T_{\text{min}}}$

c) Compare  $e_{\text{otto}}$  to  $e_{\text{Carnot}}$  where the Carnot Engine work between same  $T_{\text{max}}$  &  $T_{\text{min}}$  (temps for hot & cold reservoirs, respectively)

$$e_{\text{Carnot}} = 1 - \frac{T_c}{T_h} = 1 - \frac{T_{\text{min}}}{T_{\text{max}}} = 1 - \frac{1}{3 \cdot 5^{\gamma-1}} = 1 - \frac{5^{1-\gamma}}{3}$$

$e_{\text{otto}} = 1 - 5^{1-\gamma} < e_{\text{Carnot}} = e_{\text{max}}$   
↑ Confirms 2nd law of TD

## Entropy calculation in different processes:

(33)

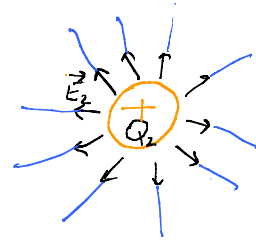
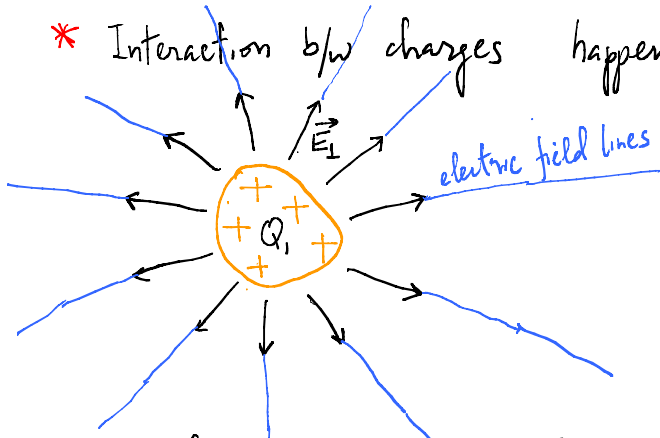
$$\Delta S \equiv \int_1^2 \frac{dQ}{T} \left\{ \begin{array}{l} \text{Isothermal: } \Delta S = \frac{1}{T} \int_1^2 dQ = \frac{Q_2 - Q_1}{T} = \frac{\Delta Q}{T} \quad (\text{change in entropy is heat change per unit temp}) \\ \text{Isovolumic: } dQ = n c_v dT \Rightarrow \Delta S = n c_v \int_1^2 \frac{dT}{T} = n c_v \ln\left(\frac{T_2}{T_1}\right) \\ \text{Isobaric: } dQ = n c_p dT \Rightarrow \Delta S = n c_p \ln\left(\frac{T_2}{T_1}\right) \end{array} \right.$$

# Ch 20: Electric Charge, Force, Field

An electric charge distribution creates an electric field, when a probe (another charge) comes to its proximity it will feel an electric force by the original charge distribution

$$\vec{F}_{12} = Q_2 \vec{E}_1$$

\* Interaction b/w charges happens through their electric fields



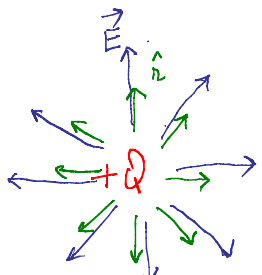
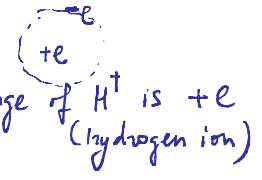
$Q_1$  = a scalar (unit is C for Coulomb)  
 $\vec{E}_1$  = a vector  
 Electric field lines point away from a + charge distribution and they are more spread out away from the charge showing  $\vec{E}_1$  is weaker away from the charge (stronger closer to charge)  
 Strength of field = density of field lines!

$Q_2$  = probe charge  
 ↳ feels  $\vec{F}_{12} = Q_2 \vec{E}_1$  (N)  
 ↳ force by ① on ②  
 $\vec{E}_2$  : electric field by  $Q_2$  ↳ unit:  $\frac{N}{C}$   
 ↳  $Q_1$  feels  $\vec{F}_{21} = Q_1 \vec{E}_2$   
 ↳ force by ② on ①  
 ⇒ Both great & host charges feel electric interaction!

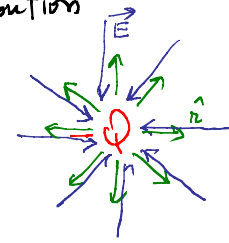
Charges { 2 types: + and -; unit = charge of electron  $e = 1.6 \cdot 10^{-19} C$  }  
 { charge of an electron is  $-e$   
 { charge of a proton is  $+e$   
 { charge of a deuteron is  $+2e$   
 { charge of a H atom: 0

"Sources" of electric field  
 Charge  $Q \rightarrow \vec{E} = k \frac{Q}{r^2} \hat{r}$

- $k$ : electric constant =  $9 \cdot 10^9 \frac{Nm^2}{C^2}$
- $Q$ : net charge of the source
- $r$ : separation from charge  $Q$  to field point or probe point (where the field is measured)
- $\hat{r}$ : radial unit vector, points away from the charge distribution



$\vec{E} = +k \frac{Q}{r^2} \hat{r}$   
 points away from charge or repulsive



$\vec{E} = -k \frac{Q}{r^2} \hat{r}$   
 points toward charge or attractive



Electric

Sources: 2 types of charges

Fields: repulsive or attractive

$$\vec{E} = k \frac{Q}{r^2} \hat{r}$$

$$k = 9 \cdot 10^9 \frac{\text{Nm}^2}{\text{C}^2}$$

Gravitational

Source: one type of mass

Fields: always attractive

$$\vec{g} = -G \frac{M}{r^2} \hat{r}$$

$$G = 6.67 \cdot 10^{-11} \frac{\text{Nm}^2}{\text{kg}^2}$$

$$\frac{k}{G} \sim 10^{20} !$$

electric interactions are huge  
compared to gravitational interactions!

We feel grav. attraction, not much electric interaction  
(one type, weak)

(two opposite types of charges  
balanced  $\rightarrow$  no fields, although  
very strong)

Calculation of the electric field  $\vec{E}$ : 3 methods:

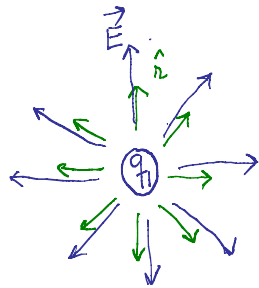
- 1) Vector superposition:
  - (i)  $\vec{E}$  by two + charges
  - (ii)  $\vec{E}$  by a ring of charge
  - (iii)  $\vec{E}$  by an  $\infty$ -long line of charge
 (ch. 20)  
 (any charge distribution)

- 2) Use Gauss' Law: use symmetry to determine the Gaussian surface  
 (ch. 21)  $\rightarrow \left\{ \begin{array}{l} \Phi_{G\text{-surface}} = \frac{q_{\text{enclosed}}}{\epsilon_0} ; \epsilon_0 = \frac{1}{4\pi \cdot k} = 8.85 \cdot 10^{-12} \frac{C^2}{Nm^2} \\ \Phi = \int \vec{E} \cdot d\vec{A} \quad \text{electric flux} \end{array} \right.$   
 (symmetric charge distribution: spherical, cylindrical, ...)

- 3) Use electric potential  $V$ , which is a scalar  $\rightarrow$  arithmetic addition (advantage)  
 (ch. 22)  $\rightarrow \vec{E} = -\vec{\nabla} V$  ;  $\vec{\nabla}$ : "gradient operator"  
 (any charge distribution) in Cartesian coords:  $\vec{\nabla} = \hat{i} \frac{\partial}{\partial x} + \hat{j} \frac{\partial}{\partial y} + \hat{k} \frac{\partial}{\partial z}$

Calculation of  $\vec{E}$  using vector superposition:

- 1)  $\vec{E}$  due to a single charge  $q_1$  :  $\vec{E} = k \frac{q_1}{r^2} \hat{r}$   
 $q_1 > 0$

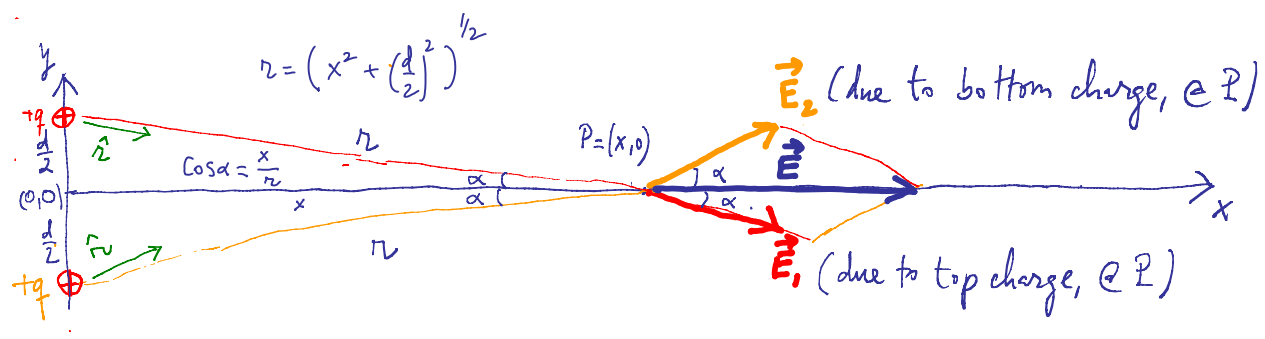


$\vec{E} = +k \frac{q_1}{r^2} \hat{r}$   
 points away from charge or repulsive

- (i) Field points in the radial direction away from a positive charge
  - (ii) Field strength is proportional to the charge  $q_1$
  - (iii) Field strength is inversely proportional to separation  $r^2$
- (both grav. & electric fields are inverse-squared law)

- 2)  $\vec{E}$  due to two positive charges : vector superposition:

$\rightarrow$  along their line of symmetry (midline b/w the two charges)



- a)  $\vec{E}_1$  &  $\vec{E}_2$  point along different directions
- b) Both have the same field strength:  $\frac{kq}{r^2}$
- c) Total field due to both charges:

$\vec{E} = \vec{E}_1 + \vec{E}_2$  { (i) Graphical vector addition: in the parallelogram formed by two adding vectors, the diagonal is the sum vector  
 (ii) Mathematically using unit vectors + component

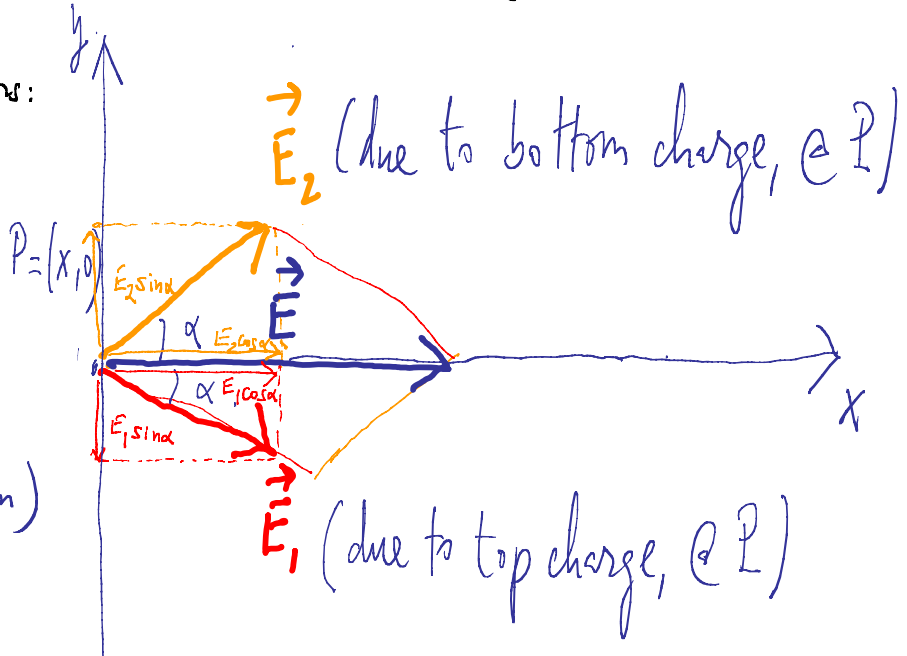
Using cartesian components & unit vectors:

$$\vec{E}_1 = E_1 \cos \alpha \hat{i} - E_1 \sin \alpha \hat{j}$$

$$+ \vec{E}_2 = E_2 \cos \alpha \hat{i} + E_2 \sin \alpha \hat{j}$$

$E_1 = E_2 = \frac{kq}{r^2}$  same strength

$$\vec{E} = 2E_1 \cos \alpha \hat{i} \quad (\text{diagonal of parallelogram in the diagram})$$



Electric field due to two positive charges along their midline:

$$\vec{E} = 2E_1 \cos \alpha \hat{i} = 2 \frac{kq}{r^2} \cdot \frac{x}{r} \hat{i} = \frac{2kqx}{r^3} \hat{i} = \frac{2kqx}{(x^2 + (\frac{d}{2})^2)^{3/2}} \hat{i} \quad \left(\frac{N}{C}\right)$$

$E_1 = E_2 = \frac{kq}{r^2}$        $\cos \alpha = \frac{x}{r}$        $r = (x^2 + (\frac{d}{2})^2)^{1/2}$

(i) Total field points along midline; field strength is  $\frac{2kqx}{(x^2 + (\frac{d}{2})^2)^{3/2}}$

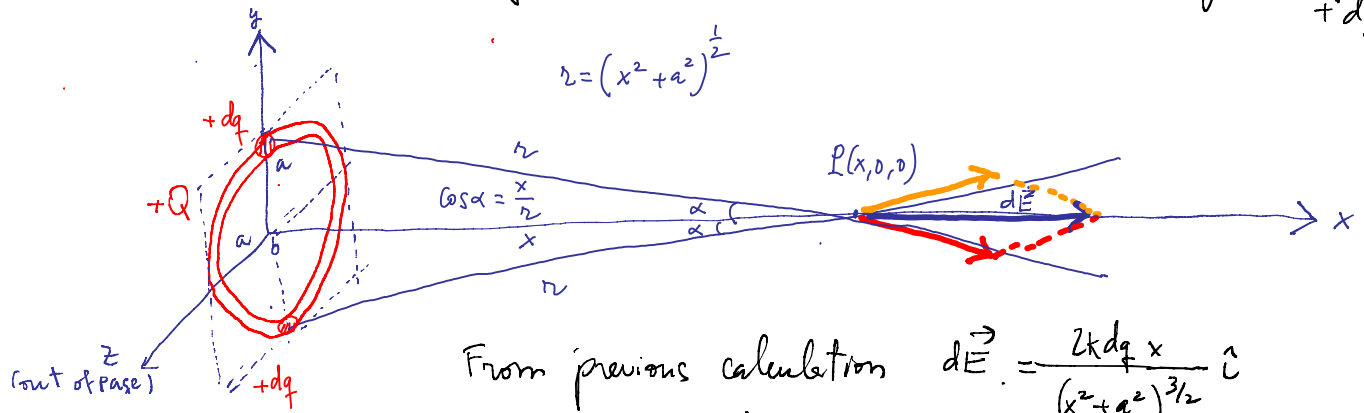
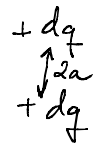
(ii) When  $P$  is very far away from the two charges ( $x \rightarrow \infty$ )

$$E \xrightarrow{x \rightarrow \infty} \frac{2kqx}{(x^2)^{3/2}} = \frac{2kqx}{x^3} = \frac{2kq}{x^2} = \frac{k(2q)}{x^2}$$

Very far away, the total field is that of a single charge of value  $2q$  (this limit makes sense!)

3) Electric field due to a continuous ring of charge @ a point  $P$  along its axis: vector superposition:

- ↳ (i) Ring in  $YZ$  plane centered in the  $x$ -axis, radius  $a$
- (ii) Ring center is origin of coordinates
- (iii) Total charge on ring is  $Q$
- (iv) Make use of total field due to two positive charges:



From previous calculation  $d\vec{E} = \frac{2kdq x}{(x^2 + a^2)^{3/2}} \hat{i}$

Field due to entire ring:  $\vec{E} = \int_{\text{half ring}} d\vec{E} = \frac{2kx}{(x^2 + a^2)^{3/2}} \hat{i} \int_{\text{half ring}} dq$

$\frac{Q}{2}$

$$\vec{E} = \frac{kQx}{(x^2 + a^2)^{3/2}} \hat{i}$$

↳ Very far away from ring  $x \gg a \rightarrow x^2 + a^2 \approx x^2$

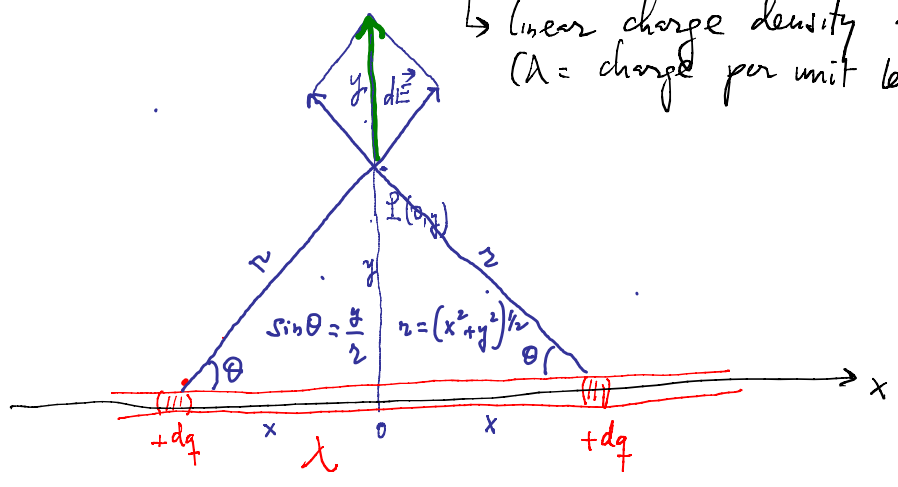
$$\vec{E} = \frac{kQx}{(x^2)^{3/2}} \hat{i} = \frac{kQx}{x^3} \hat{i} = \frac{kQ}{x^2} \hat{i}$$

Makes sense

Very far away from ring it looks like a single charge of value  $Q$

4) Electric field due to  $\infty$ -long line of charge

↳ linear charge density  $\lambda \equiv \frac{dq}{dx}$   
 ( $\lambda$  = charge per unit length)



Set up  $+dq \leftarrow \frac{x}{r} \rightarrow +dq$  so to use results 2)  $\vec{E}$  due to two positive charges at a point P along their midline:  $d\vec{E} = \frac{2k dq}{r^2} \sin\theta \hat{j} = \frac{2k dq y}{r^3} \hat{j} = \frac{2k \lambda dx \cdot y}{(x^2+y^2)^{3/2}} \hat{j}$   
 $\lambda = \frac{dq}{dx} \Rightarrow dq = \lambda dx$

Total field  $\rightarrow$  vector superposition: integral over half line:

$$\vec{E} = \int_{\text{Half line}} d\vec{E} = 2k\lambda y \hat{j} \int_{\text{Half line}} \frac{dx}{(x^2+y^2)^{3/2}} = 2k\lambda y \hat{j} \left[ \frac{x}{y^2(x^2+y^2)^{1/2}} \right]_0^{\infty}$$

$x \rightarrow \infty \quad (x^2+y^2)^{1/2} \rightarrow (x^2)^{1/2} = x$

$$\vec{E} = 2k\lambda y \hat{j} \frac{x}{y^2 \cdot x} = \frac{2k\lambda}{y} \hat{j}$$

Note: here field is inverse-linear Law not inverse-squared Law!

# Ch 21 Gauss Law :

$$\hookrightarrow \phi_{G\text{-surface}} = \frac{q_{\text{enclosed}}}{\epsilon_0} ; \epsilon_0 = \text{dielectric constant in vacuum}$$

$$= \frac{1}{4\pi k} = 8.85 \cdot 10^{-12} \frac{C^2}{Nm^2}$$

$\phi_{G\text{-surface}}$  : electric flux through Gaussian surface.

$$\phi = \oint_{\text{closed surface}} \vec{E} \cdot d\vec{A}$$

↑ dot product  
= scalar product

$\vec{E}$  : electric field  
 $d\vec{A}$  : element area of surface we integrate over. always points away from surface  
 $\vec{E} \cdot d\vec{A}$  : electric flux element  $\rightarrow \int \vec{E} \cdot d\vec{A} \rightarrow$  total electric flux through closed surface

$\vec{A} \cdot \vec{B} = AB \cos \theta$   
 $\theta$  : angle b/w  $\vec{A}$  &  $\vec{B}$   
 only if  $\vec{A} \parallel \vec{B} \Rightarrow \theta = 0^\circ$   
 $\Rightarrow \cos \theta = 1 \Rightarrow \vec{A} \cdot \vec{B} = A \cdot B$   
 (scalar product is reduced to arithmetic product)

Gaussian surface : a closed surface such that

- Goals
- (i) Make  $\phi = \oint \vec{E} \cdot d\vec{A}$  simply  $E \cdot A$
  - (ii) This allows us to use Gauss Law to calculate  $E$  :

$$\oint \vec{E} \cdot d\vec{A} = E \cdot A$$

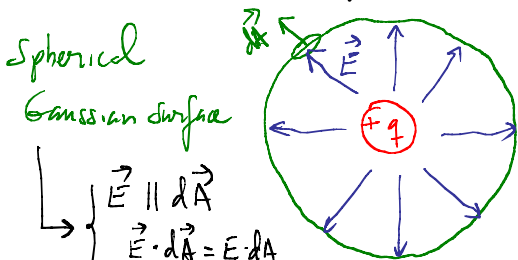
$\int E$  is constant over Gaussian surface  $\rightarrow \vec{E} \parallel d\vec{A}$

Requirement: **Symmetric charge distribution!**

$$\phi_{G\text{-surface}} = \frac{q_{\text{enclosed}}}{\epsilon_0}$$

$$E \cdot A = \frac{q_{\text{enclosed}}}{\epsilon_0} \Rightarrow E = \frac{q_{\text{enclosed}}}{\epsilon_0 \cdot A}$$

$\vec{E}$  due to a single charge :



$A = 4\pi r^2$  (surface of a sphere of radius  $r$ )

$\epsilon_0 = \frac{1}{4\pi k} \rightarrow 4\pi \epsilon_0 = \frac{1}{k}$

inverse-square law : same separation  $r$ , same field strength  $\rightarrow E$  is constant over Gaussian surface :  $\phi = \oint \vec{E} \cdot d\vec{A} = \oint E \cdot dA = E \oint dA = E \cdot A$

$\rightarrow$  Gauss Law :

$$\phi = \frac{q_{\text{enclosed}}}{\epsilon_0}$$

$$E \cdot A = \frac{q}{\epsilon_0} \Rightarrow E = \frac{q}{\epsilon_0 A} = \frac{q}{4\pi \epsilon_0 r^2} = \frac{q}{\frac{1}{k} r^2}$$

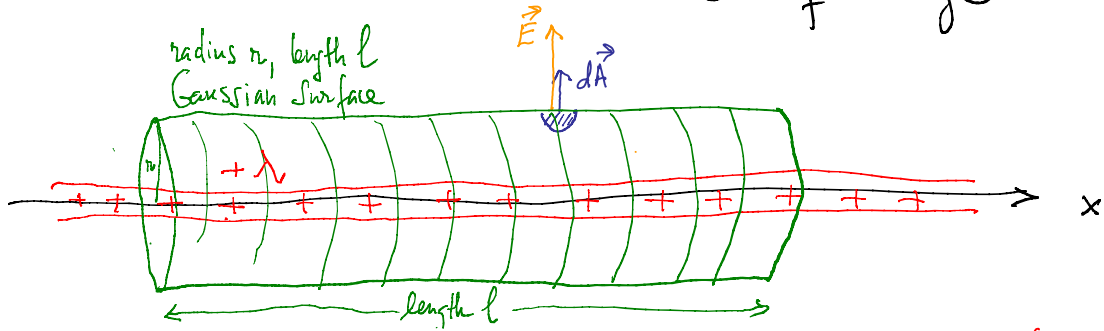
$$= \frac{kq}{r^2} \checkmark$$

Calculation of  $\vec{E}$  by an  $\infty$ -long line of charge (linear charge density  $\lambda \equiv \frac{dq}{dx}$ )

↳ Using Gauss Law

↳ Symmetry of charge distribution

↳ Cylindrical Gaussian surface whose axis is the line of charge



With this Gaussian surface:

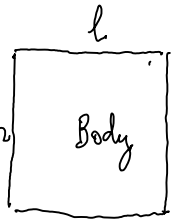
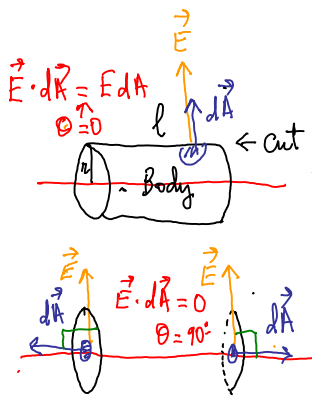
- (i)  $d\vec{A} \parallel \vec{E} \Rightarrow \vec{E} \cdot d\vec{A} = E dA$  (both  $\vec{E}$  &  $d\vec{A}$  point in the radial direction & away from line of charge)
- (ii)  $\vec{E}$  has same strength on surface (same separation  $r$  to line of charge)

$\Rightarrow \phi = \oint \vec{E} \cdot d\vec{A} = E \oint dA = EA$

(iii) Total surface area of the cylinder of radius  $r$  & length  $l$  is:  $2\pi r \cdot l + \pi r^2 + \pi r^2$

(iv) enclosed by G-surface:  $\lambda \cdot l$

don't count for  $\phi$  as  $\vec{E} \cdot d\vec{A} = 0$  on left & right sides (see diagrams on left)



Gauss Law =  $\phi = \frac{q_{\text{enclosed}}}{\epsilon_0}$

$\downarrow$   
 $EA$   
 $\downarrow$   
 $E \cdot 2\pi r l = \frac{\lambda \cdot l}{\epsilon_0} \Rightarrow E = \frac{\lambda}{2\pi \epsilon_0 r} = \frac{\lambda}{2\pi \cdot \frac{1}{4\pi k} r} = \frac{2k\lambda}{r}$

(same result as using Vector superposition)

# Ch 22 Electric Potential

(3<sup>rd</sup> method to calculate  $\vec{E}$ )

Mechanics: potential energy (difference) b/w two points A & B:

$$\Delta U_{AB} = - \int_A^B \vec{F} \cdot d\vec{l}$$

scalar product

(i)  $\vec{F} = m\vec{g}$  or  $G \frac{Mm}{r^2} \hat{r} \rightarrow \Delta U$  is grav. potential energy  
 (ii)  $\vec{F} = q'\vec{E}$   $\rightarrow \Delta U$  is electric potential energy  
 probe charge

$$\rightarrow \Delta U_{AB} = -q' \int_A^B \vec{E} \cdot d\vec{l}$$

$\rightarrow \Delta V_{AB} \equiv \frac{\Delta U_{AB}}{q'}$  : electric potential (difference) b/w two points A & B  
 unit is  $\frac{J}{C}$

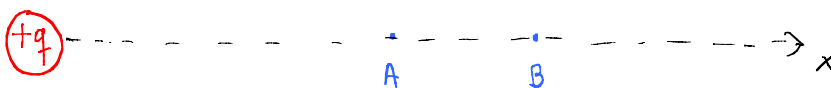
$$\Delta V_{AB} = - \int_A^B \vec{E} \cdot d\vec{l}$$

$$\Rightarrow \vec{E} = - \vec{\nabla} V_{AB}$$

gradient: vector derivative

Calculate  $\vec{E}$  due to a point charge using electric potential (difference):

$$d\vec{l} = dx \hat{i}$$



$$(i) \Delta V_{AB} = - \int_A^B \frac{kq}{x^2} \hat{i} \cdot \hat{i} dx = -kq \int_A^B \frac{dx}{x^2} = kq \left[ \frac{1}{x} \right]_A^B = kq \left[ \frac{1}{x_B} - \frac{1}{x_A} \right]$$

$1 \cdot 1 \cdot \cos 0 = 1$

Define:  $V \equiv \frac{kq}{x} \Rightarrow \Delta V_{AB} = V_B - V_A$

(ii) Set reference for electric potential  $V=0$  @  $x=\infty \Rightarrow V_\infty = \frac{kq}{\infty} = 0$

$$\Delta V_{\infty B} = V_B - V_\infty = V_B \Rightarrow V_r \equiv \Delta V_{\infty r}$$

$$V(r) = \frac{kq}{r}$$

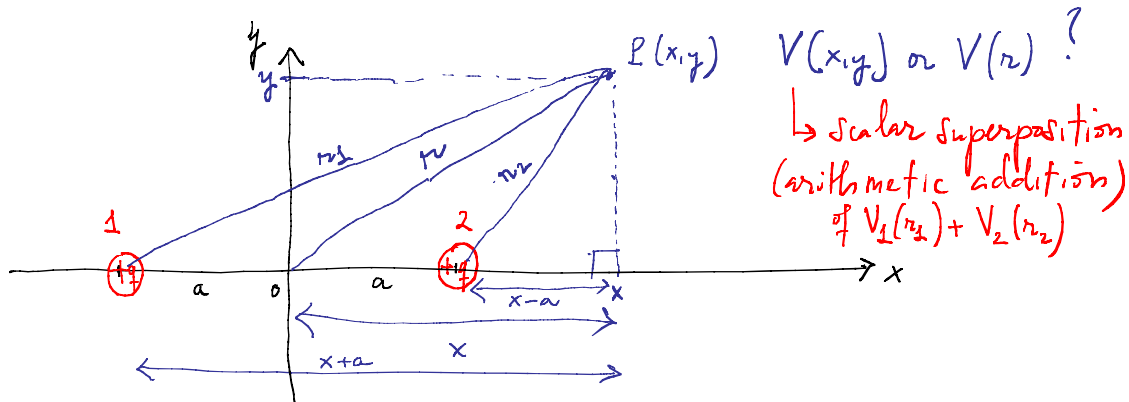
Electric potential due to a point charge  $q$  at separation  $r$  from charge.



(iii)  $E(r) = -\nabla V = -\frac{d}{dr} V = -\frac{d}{dr} \left( \frac{kq}{r} \right) = -kq \frac{d}{dr} \left( \frac{1}{r} \right) = \frac{kq}{r^2}$  ✓ (43)

22.52

Electric potential for 2 identical charges at  $x = \pm a$  at any point  $P(x, y)$



a)  $V(r) = V_1(r_1) + V_2(r_2)$

$$= \frac{kq}{r_1} + \frac{kq}{r_2} = kq \left[ \frac{1}{\sqrt{(x+a)^2 + y^2}} + \frac{1}{\sqrt{(x-a)^2 + y^2}} \right]$$

b) Very far away from the two charges:  $x \gg a$  or  $x+a \approx x$  and  $x-a \approx x$   
 ↳ the two denominators are identical:

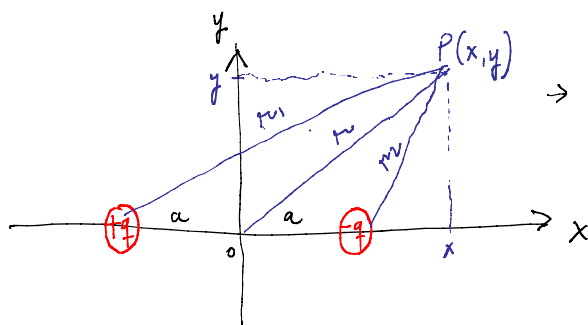
$$V(r) = \frac{2kq}{\sqrt{x^2 + y^2}} = \frac{2kq}{r} = k \frac{(2q)}{r}$$

22.53

Electric potential for a dipole

A dipole consists of two identical charges of opposite signs separated by a distance  $2a$

$+q \quad a \quad a \quad -q \Rightarrow$  electric dipole moment  $p \equiv q \cdot 2a$

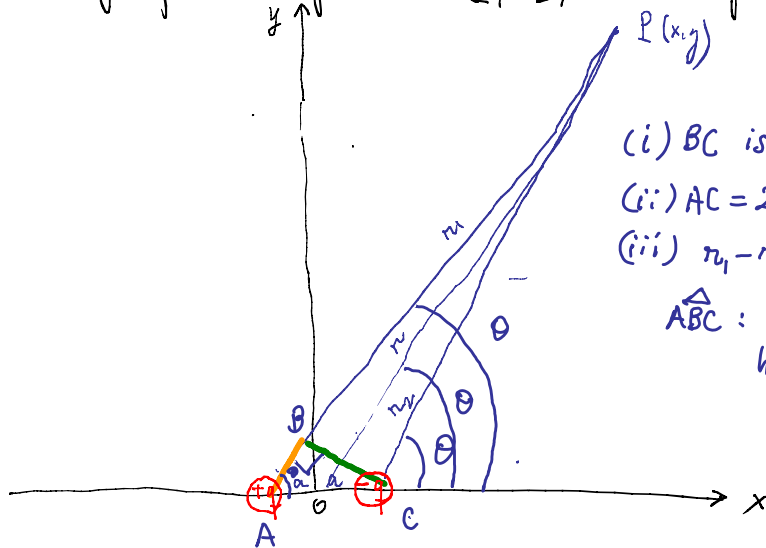


$\rightarrow V(x, y)$  or  $V(r) = V_1(r_1) + V_2(r_2)$

$$= \frac{kq}{r_1} - \frac{kq}{r_2}$$

$$V(r) = kq \left( \frac{1}{r_1} - \frac{1}{r_2} \right) = kq \frac{r_2 - r_1}{r_1 r_2}$$

Very far away from dipole:  $r_1, r_2, r$  are parallel to each other: (44)



(i) BC is  $\perp$  to all three lines

(ii)  $AC = 2a$

(iii)  $r_1 - r_2 = AB = AC \cdot \cos \theta = 2a \cos \theta$

$\triangle ABC$ : right  $\angle$   
hypotenuse is  $AC = 2a$

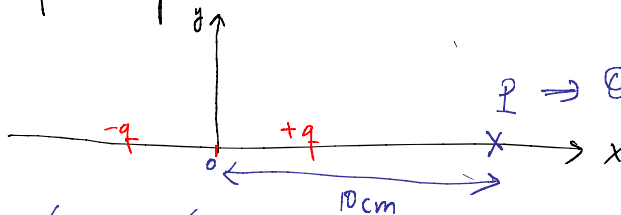
$$V(r) = kq \frac{r_2 - r_1}{r_1 r_2} \approx -kq \frac{2a \cos \theta}{r^2} = -\frac{kp \cos \theta}{r^2} *$$

very far away from dipole
 $p = q \cdot 2a$

\* If  $-q$  is on left &  $+q$  on right  $V(r) = kq \left( \frac{1}{r_2} - \frac{1}{r_1} \right) = kq \frac{r_1 - r_2}{r_1 r_2} \approx kq \frac{2a \cos \theta}{r^2} = +\frac{kp \cos \theta}{r^2}$

If  $p = 2.9 \text{ nC}\cdot\text{m}$  ( $2a \ll 10 \text{ cm} \rightarrow$  Very far away approx. !)

a)  $V?$  10cm from dipole on its axis



$p \Rightarrow \theta = 0^\circ$   $V = \frac{kp}{r^2} = \frac{kp}{x^2}$   
on axis

$$V = \frac{9 \cdot 10^9 \cdot 2.9 \cdot 10^{-9}}{0.1^2} = 26.1 \cdot 10^2 \text{ V} = 2.61 \cdot 10^3 \text{ V} = 2.61 \text{ kV}$$

(Volt, SI unit for electric potential)

b)  $V(\theta = 45^\circ) = \frac{9 \cdot 10^9 \cdot 2.9 \cdot 10^{-9} \cdot \cos 45^\circ}{0.1^2} \text{ V}$

c)  $V(\text{on } \perp \text{ bisector}) = 0$   
 $\theta = 90^\circ$

22.31 | Given  $V(x,y,z) = 2xy - 3zx + 5y^2$  (V)

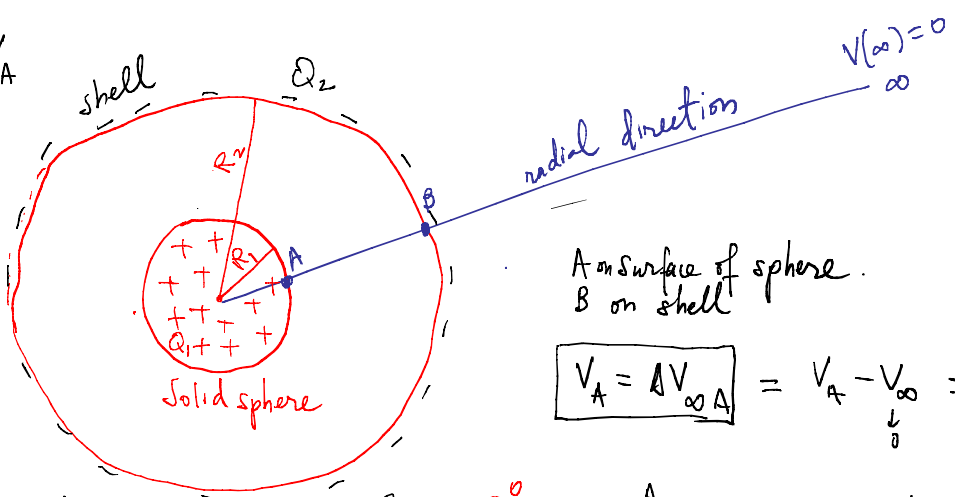
a)  $V(1,1,1) = 2 - 3 + 5 = 4 \text{ V}$

b)  $\vec{E}(x,y,z) = -\vec{\nabla} V = -\frac{\partial V}{\partial x} \hat{i} - \frac{\partial V}{\partial y} \hat{j} - \frac{\partial V}{\partial z} \hat{k} = -(2y - 3z) \hat{i} - (2x + 10y) \hat{j} + 3x \hat{k}$

$\vec{E}(1\text{m}, 1\text{m}, 1\text{m}) = -(-1) \hat{i} - (12) \hat{j} + 3 \hat{k} = \hat{i} - 12 \hat{j} + 3 \hat{k}$  ( $\frac{\text{N}}{\text{C}}$ )

22.67 | a) Find  $V_A$

$Q_1 = 60 \text{ nC}$   
 $R_1 = 0.05 \text{ m}$   
 $Q_2 = -60 \text{ nC}$   
 $R_2 = 0.15 \text{ m}$   
 Reference potential  
 $V=0 @ \infty$



A on surface of sphere.  
 B on shell  
 $V_A = \Delta V_{\infty A} = V_A - V_{\infty} = V_A$

$$V_A = \Delta V_{\infty A} = - \int_{\infty}^A \vec{E} \cdot d\vec{l} = - \int_{\infty}^B \vec{E} \cdot d\vec{r} - \int_B^A \vec{E} \cdot d\vec{r} = - \int_B^A \frac{kQ_1}{r^2} \hat{r} \cdot \hat{r} dr$$

outside shell  $Q = Q_1 + Q_2 = 0$   
 $\vec{E} = 0$   
 b/w sphere & shell  
 $\vec{E} = \frac{kQ_1}{r^2} \hat{r}$

Notes } Gauss Law:  $EA = \frac{q_{\text{enclosed}}}{\epsilon_0}$   
 (only charge enclosed creates E)  
 $d\vec{r} = dr \hat{r}$

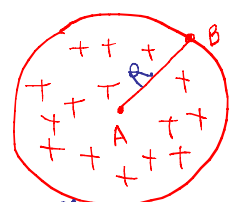
$$V_A = -kQ_1 \int_B^A \frac{dr}{r^2} = kQ_1 \left[ \frac{1}{r_A} - \frac{1}{r_B} \right] = 9 \cdot 10^9 \cdot 60 \cdot 10^{-9} \left[ \frac{1}{0.05} - \frac{1}{0.15} \right] = 7.2 \text{ kV}$$

b) Now shell carries  $+60 \text{ nC}$

$$V_A = - \int_{\infty}^B \frac{k(Q_1 + Q_2)}{r^2} dr + V_A(a) = +k(Q_1 + Q_2) \left[ \frac{1}{r_B} - \frac{1}{r_{\infty}} \right] + 7.2 \text{ kV}$$

$$= 9 \cdot 10^9 \cdot 120 \cdot 10^{-9} \frac{1}{0.15} + 7.2 \text{ kV} = 14.4 \text{ kV}$$

22.65 | Sphere of radius R &  $\vec{E} = E_0 \left( \frac{r}{R} \right)^2 \hat{r}$  ( $0 < r < R$ )  
 ↑  
 inside sphere



A @ center  $r_A = 0$   
 B @ surface  $r_B = R$   
 $\Delta V_{BA}$  ? potential surface to center

$$\Delta V_{BA} = - \int_B^A \vec{E} \cdot d\vec{r} = - \frac{E_0}{R^2} \int_B^A r^2 dr = - \frac{E_0}{R^2} \left[ \frac{r^3}{3} \right]_B^A = - \frac{E_0}{R^2} \left[ 0 - \frac{R^3}{3} \right] = \frac{E_0 R}{3}$$

Gauss LawElectric

$$\Phi = \oint_{\text{Gaussian surface}} \vec{E} \cdot d\vec{A} = \frac{q_{\text{enclosed}}}{\epsilon_0}$$

by G-surface

Grav.

$$\Phi_g = \oint_{\text{Gaussian surface}} \vec{g} \cdot d\vec{A} = -4\pi G M_{\text{enclosed}}$$

by G-surface

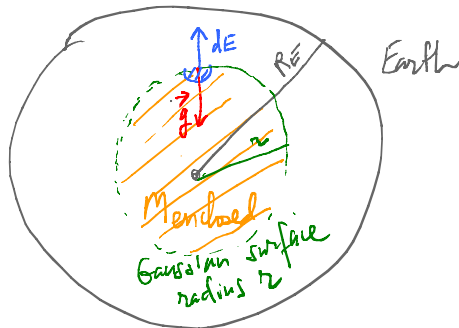
Univ. grav. constant

Prove  $g(r) = g_0 \frac{r}{R_E}$  ( $0 < r < R_E$ ) inside Earth.

Use Gauss Law to calculate field (grav. or electric)

(i) Choose Gaussian surface: symmetry of charge or mass distributions

↳ Earth → spherical



$$\frac{M_{\text{enclosed}}}{M_E} = \frac{\frac{4\pi}{3} r^3}{\frac{4\pi}{3} R_E^3} \Rightarrow M_{\text{enclosed}} = M_E \frac{r^3}{R_E^3}$$

(ii)  $d\vec{A}$  points in radial direction away from G-surface  
 $\vec{g}$  " " " " " towards center of G-surface }  $\theta = 180^\circ$   
 $\cos 180^\circ = -1$

$$\vec{g} \cdot d\vec{A} = -g dA$$

(iii) Due to spherical symmetry  $g$  is constant on G-surface

$$\Phi_g = \oint \vec{g} \cdot d\vec{A} = -g \oint dA = -g 4\pi r^2$$

(iv) Gauss Law for grav. field:  $\Phi_g = -4\pi G M_{\text{enclosed}}$ 

$$-g 4\pi r^2 = -4\pi G M_E \frac{r^3}{R_E^3}$$

$$g = \frac{G M_E}{R_E^3} r \quad \text{any } 0 < r < R_E$$

(v) On surface  $r = R_E \Rightarrow g(R_E) = g_0 = \frac{G M_E}{R_E^3} R_E = \frac{G M_E}{R_E^2} = 9.81 \frac{\text{m}}{\text{s}^2}$

$$\Rightarrow g(r) = \frac{GM_E}{R_E^2} \frac{r}{R_E} = g_0 \frac{r}{R_E} \quad \checkmark$$