

Ch 12: Static Equilibrium

Application of force & torque balance:

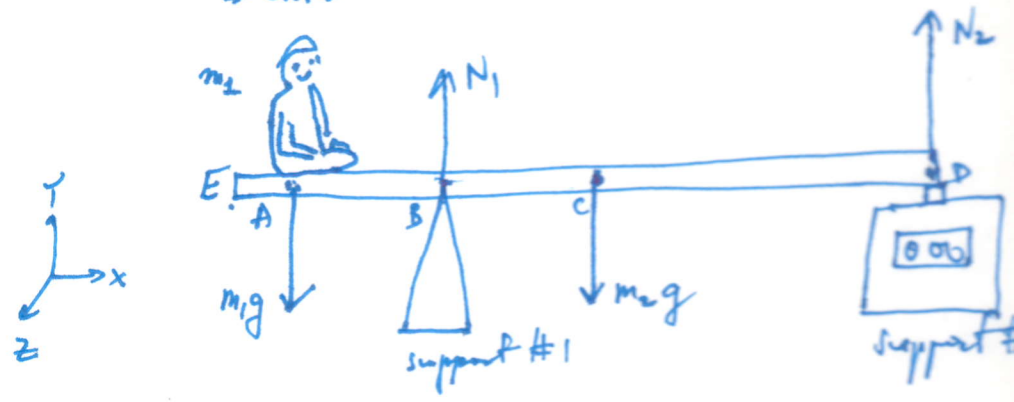
Static equilibrium

- 1) $\sum_i \vec{F}_i = 0$ (No net force on object)
- 2) $\sum_i \vec{\tau}_i = 0$ (No net torque on object)

↳ if it will not move neither rotate

12.22

→ Scale: 3 parts, beam & 2 supports.
 → child where does he sit so support #2 "feels"



support #2 "feels"
 a) 100N
 b) 300N

data | Child: $m_1 = 40\text{kg}$
 beam: $m_2 = 50\text{kg}$
 $ED = L = 2.4\text{m}$
 S_2 is 0.8m from left end.
 $EB = 0.8\text{m}$
 $EC = 1.2\text{m} = CD$

→ Focus on beam: which should be in static equilibrium when a reading is taken.

↳ $\sum_i \vec{F}_i = 0$ (on beam!)
 ↳ $\sum_i \vec{\tau}_i = 0$ (on beam!)

Forces on beam: child's weight m_1g ; beam's weight m_2g .
 + normal forces by supports on beam: N_1 & N_2

↳ $\sum_i \vec{F}_i = 0: N_1 + N_2 - m_1g - m_2g = 0$

Torques on beam: torque definition requires a pivot, what is it? for the calculations: any force application point (there are 4) will do →
 If there is a force we don't know or don't care about → pivot at its application point
 ... due to that force is 0!

In this problem we don't want to place the pivot at A neither D. \rightarrow B or C, since we know m_2 , but not $N_1 \rightarrow$ (B).

Any force applying on a pivot contributes no torque!
 \rightarrow 3 torques:

$$\sum_i \vec{\tau}_i = 0 \rightarrow \vec{\tau}_1 + \vec{\tau}_2 + \vec{\tau}_{S2} = 0$$

from child
from beam
from support #2

$$\vec{\tau}_1 = r_{BA} m_1 g \hat{k} \quad \vec{\tau}_2 = r_{BC} m_2 g (-\hat{k})$$

$$\vec{\tau}_{S2} = r_{BD} N_2 \hat{k}$$

$$\underbrace{(r_{BA} m_1 g - r_{BC} m_2 g + r_{BD} N_2)}_0 \hat{k} = 0$$

$$r_{BA} = \frac{r_{BC} m_2 g - r_{BD} N_2}{m_1 g}$$



$\Rightarrow r_{BC} = 0.4 \text{ m}$

$\Rightarrow r_{BD} = 1.6 \text{ m}$

$N_2 = 100 \text{ N} \approx 300 \text{ N}$ by action & reaction (3rd Newton's law)

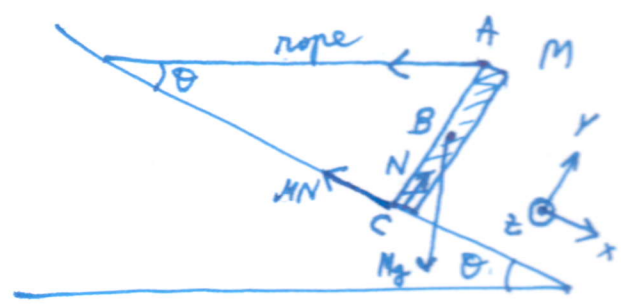
c) $r_{BA} = \frac{0.4 \times 60 \times 9.81 - 1.6 \times 100}{40 \times 9.81} = 0.19 \text{ m}$

Child sits @ 0.19m from pivot point B.
 or 0.61m from left end E

$$d) r_{BA} = \frac{0.4 \times 60 \times 9.81 - 1.6 \times 300}{40 \times 9.81} = \ominus 0.62 \text{ m}$$

child sits @ 0.62m to the right of pivot B!
 or $0.8 + 0.62 = 1.42 \text{ m}$ from left end E!

12.57



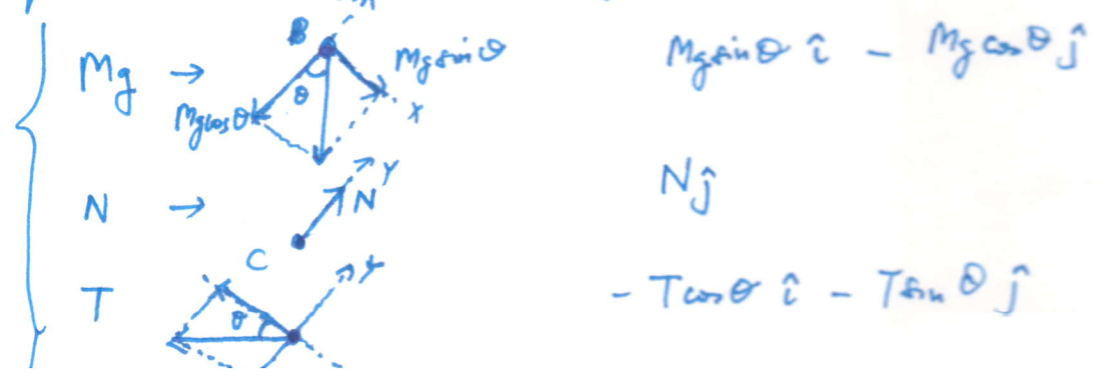
Min coef of friction b/w pole & slope for pole in static equilibrium

$$\left\{ \begin{array}{l} \sum \vec{F}_i = 0 \text{ (on pole)} \\ \sum \vec{\tau}_i = 0 \text{ (on pole)} \end{array} \right.$$

→ Forces acting on pole:

- Mg (applying on CM of pole @ B)
- N (applying @ contact point w/ slope @ C)
- T (applying @ top or point A)
- μN (applying @ contact w/ slope @ C, uphill since if there was no friction, bottom of pole would tend to slide downhill in this example)

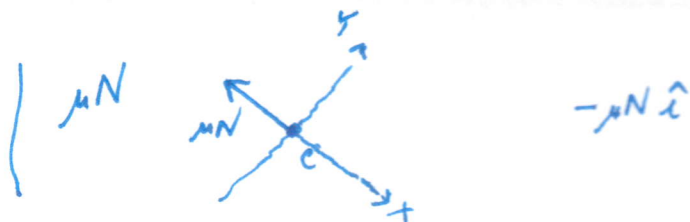
Components of these forces along coordinate axes x & y:



$$Mg \sin \theta \hat{i} - Mg \cos \theta \hat{j}$$

$$N \hat{j}$$

$$-T \cos \theta \hat{i} - T \sin \theta \hat{j}$$



1) $\sum_i \vec{F}_i = 0$ (net force on pole is zero) ①

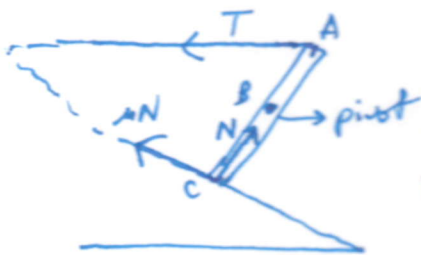
↳ $\begin{cases} x: & (Mg \sin \theta - T \cos \theta - \mu N) \hat{i} = 0 \\ y: & (-Mg \cos \theta + N - T \sin \theta) \hat{j} = 0 \end{cases}$ ②

2) $\sum_i \vec{\tau}_i = 0$ (net torque on pole is zero).

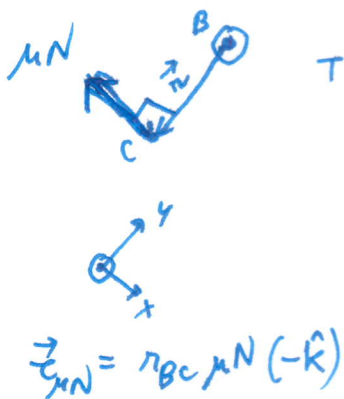
→ Pivot: CM or point B (not C: since we need friction to stay in the equation; not A since tension is related to θ , a known parameter)

↳ @ B → Mg contributes no torque. → 3 torques, effectively 2 since $\vec{\tau}_N = 0$ b/c $\vec{N} \parallel \vec{r}_{BN}$ ($\theta \neq 0 \rightarrow \sin \theta \neq 0$)

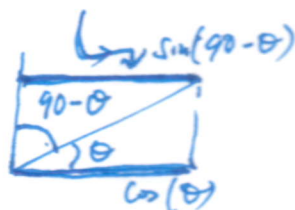
↳ $\vec{\tau}_{\mu N} + \vec{\tau}_T = 0$



$\vec{\tau}_N = \vec{r}_{BC} \times \vec{N} = 0$



$\vec{\tau}_T = r_{BA} T \sin(90 - \theta) \hat{k} = r_{BA} T \cos \theta \hat{k}$



$\sum_i \vec{\tau}_i = 0 \rightarrow (-r_{BC} \mu N + r_{BA} T \cos \theta) \hat{k} = 0$ ③

Pivot point B is CM of pole $\rightarrow r_{BC} = r_{BA}$

$-\mu N + T \cos \theta = 0$

From force & torque balance for pole:

$$\begin{cases} Mg \sin \theta - T \cos \theta - \mu N = 0 & (1) \\ -Mg \cos \theta + N - T \sin \theta = 0 & (2) \\ -\mu N + T \cos \theta = 0 & (3) \end{cases}$$

$$(3) \text{ in } (1) \rightarrow Mg \sin \theta - 2T \cos \theta = 0$$

$$T = \frac{Mg \sin \theta}{2 \cos \theta} = \frac{Mg \tan \theta}{2}$$

Use this in (2):

$$N = Mg \cos \theta + T \sin \theta$$

$$= Mg \cos \theta + \frac{Mg \tan \theta \sin \theta}{2}$$

$$= Mg \left[\cos \theta + \frac{\tan \theta \sin \theta}{2} \right]$$

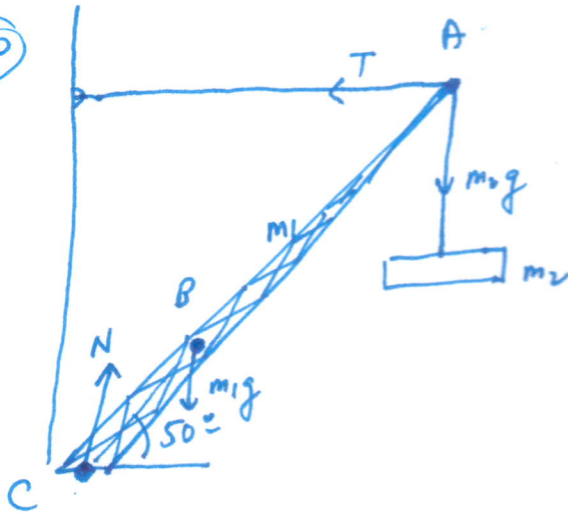
$$(3) \quad \mu = \frac{T \cos \theta}{N} = \frac{\frac{Mg}{2} \tan \theta \cos \theta}{Mg \left(\cos \theta + \frac{\tan \theta \sin \theta}{2} \right)} \quad \times \frac{2}{\cos \theta}$$

$$\quad \quad \quad \times \frac{2}{\cos \theta}$$

$$\mu = \frac{\tan \theta}{(2 + \tan^2 \theta)} \quad (\text{min})$$

$$\rightarrow \mu_s \geq \frac{\tan \theta}{2 + \tan^2 \theta}$$

12-40

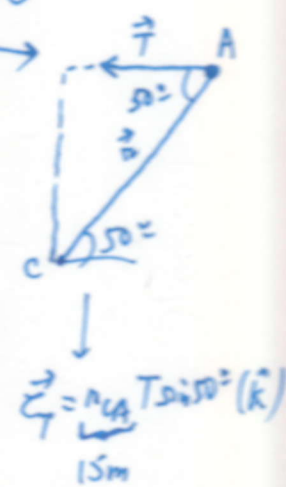
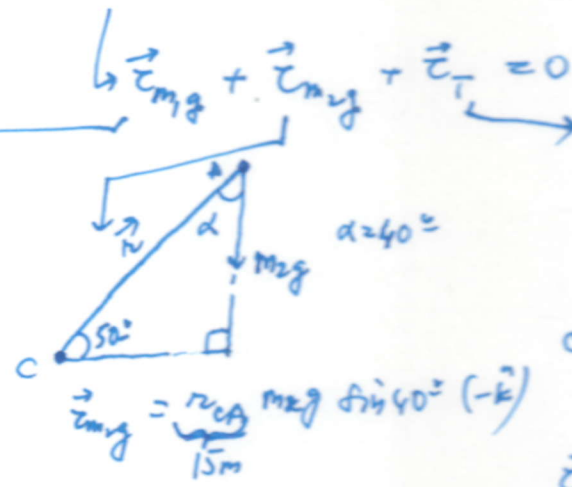
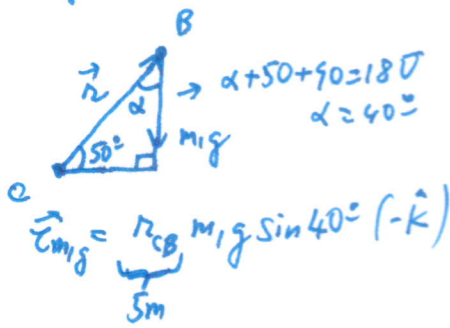
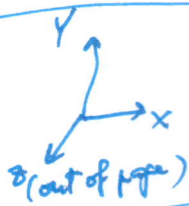


Data: CA = 15m; CB = 5m
 B @ CM of boom (mass m_1)
 $m_1 = 860 \text{ kg}$
 $m_2 = 2500 \text{ kg}$

Static equilibrium, for m_1 :

$\sum_i \vec{F}_i = 0 \rightarrow$ net force on boom is zero

$\sum_i \vec{\tau}_i = 0 \rightarrow$ proof: A B C
 we don't know N @ its angle



$$- 5 \times 860 \times 9.81 \sin 40^\circ - 15 \times 2500 \times 9.81 \sin 40^\circ + 15 T \sin 50^\circ = 0$$

$$T = \frac{5 \times 860 \times 9.81 \sin 40^\circ + 15 \times 2500 \times 9.81 \sin 40^\circ}{15 \sin 50^\circ} \text{ N}$$

$$T = 22900 \text{ N}$$

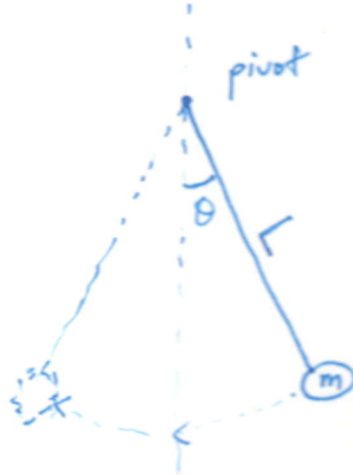
Ch 13 Oscillatory Motion

A different type of motion:

Example.

1) Pendulum

Bob attached to a string, which is attached to a fixed point or pivot. System swinging about pivot point.



Better described with an angle θ (closer to a rotation than a linear motion)

$$\tau = I\alpha \rightarrow \alpha = \frac{\tau}{I} \rightarrow \frac{d^2\theta}{dt^2} = -\frac{g}{L} \sin\theta$$

Very typical approximation is θ small \approx "small angle approximation"

$\sin\theta \approx \theta \rightarrow \frac{d^2\theta}{dt^2} = -\frac{g}{L}\theta$ 2nd Linear differential eq.

$\theta = \theta_M \cos(\omega t)$ $\left\{ \begin{array}{l} \theta_M = \text{amplitude} \\ \omega = \text{angular freq.} \end{array} \right.$

ω : # oscillations per second. What is it in terms of the length L and/or the mass of the bob m ?

Plug solution back into the equation:

$$\frac{d}{dt} \left[\frac{d}{dt} \theta_M \cos(\omega t) \right] = -\frac{g}{L} \theta_M \cos(\omega t)$$

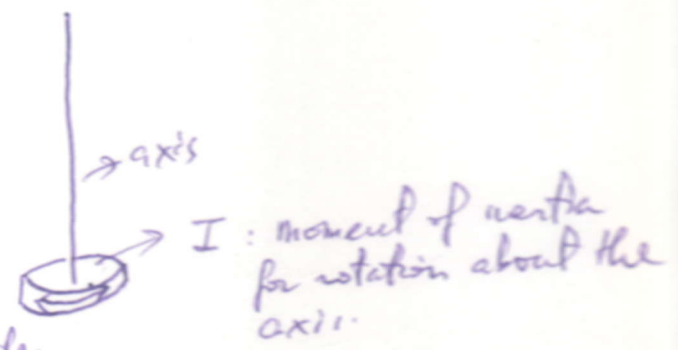
$\left(\begin{array}{l} \text{does not} \\ \text{depend on} \\ \text{time} \end{array} \right) \left(\begin{array}{l} -\theta_M \omega \sin(\omega t) \\ + \theta_M \omega^2 \cos(\omega t) \end{array} \right) = +\frac{g}{L} \theta_M \cos(\omega t) \rightarrow \omega^2 = \frac{g}{L} \rightarrow \omega = \sqrt{\frac{g}{L}}$

For a pendulum (where we can apply the "small angle approx."), the number of oscillations per second or angular frequency depends on g and L (but not on m)

$$\omega = \sqrt{\frac{g}{L}} \quad \left\{ \begin{array}{l} \text{less } \omega \text{ for longer pendulum} \\ \text{more osc. per second for shorter pendulum.} \end{array} \right.$$

2) Torsional pendulum :

Not a swinging motion, more of a twisting back & forth



$$\tau = I \alpha$$

Twisting : $\tau = -K \theta$ → twisting angle

↳ "Kappa" : torsional constant (Analog of Hooke's Law for twisting motion)

$$-K \theta = I \frac{d^2 \theta}{dt^2}$$

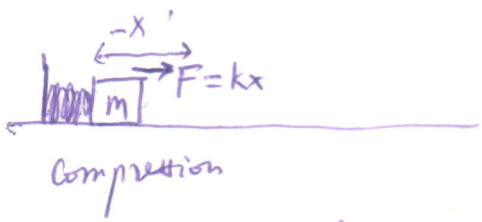
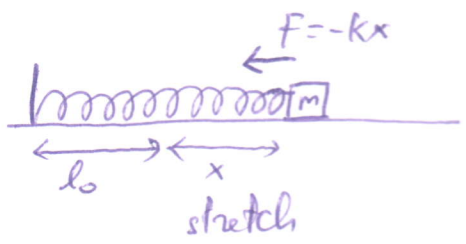
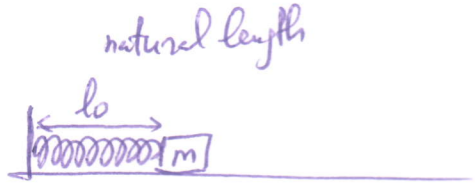
$$\rightarrow \boxed{\frac{d^2 \theta}{dt^2} = -\frac{K}{I} \theta}$$

2nd order linear differential equation

↳ $\theta = \theta_m \cos \omega t$; $\boxed{\omega = \sqrt{\frac{K}{I}}}$

↓
amplitude of oscillation

3) Spring & bob $\left\{ \begin{array}{l} k = \text{spring constant} \\ m = \text{mass of bob} \end{array} \right.$



Spring always opposes the motion of m
→ m undergoes oscillatory motion.

Newton's 2nd Law =

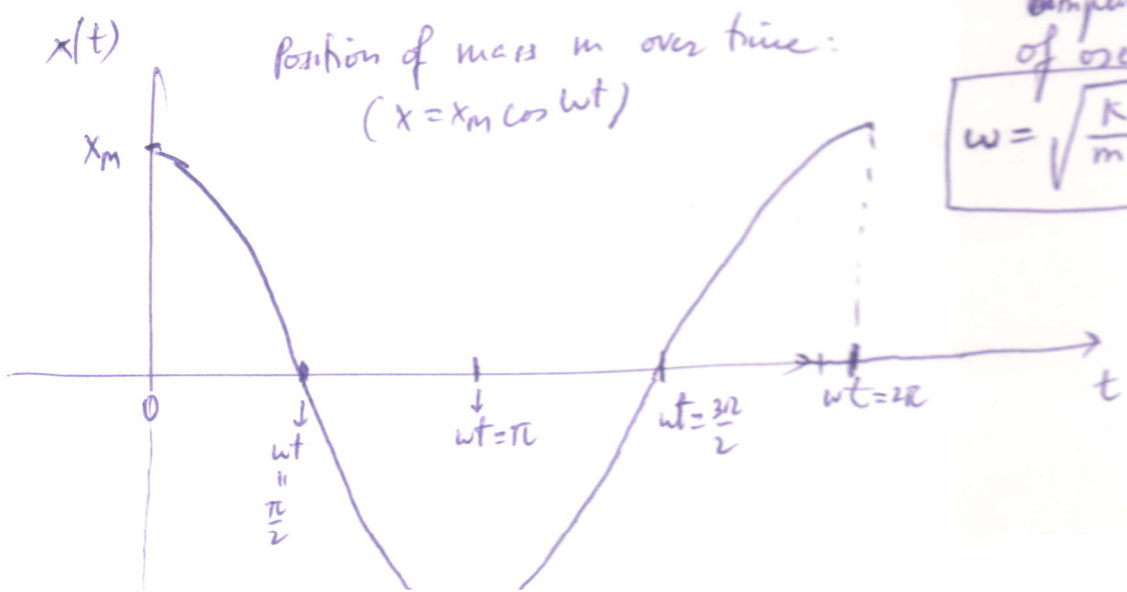
$$F = ma$$
$$-kx = m \frac{d^2x}{dt^2}$$

$$\boxed{\frac{d^2x}{dt^2} = -\frac{k}{m}x}$$
 2nd order linear differential eq.

$$\hookrightarrow x = x_m \cos(\omega t)$$

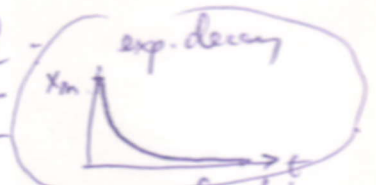
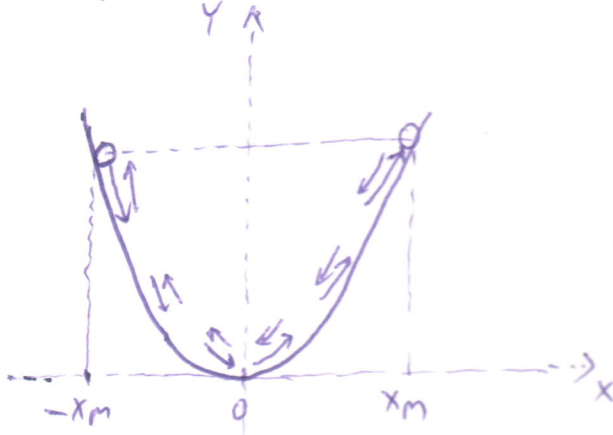
↓
amplitude of oscillation

$$\boxed{\omega = \sqrt{\frac{k}{m}}}$$



position of mass m over time:
($x = x_m \cos \omega t$)

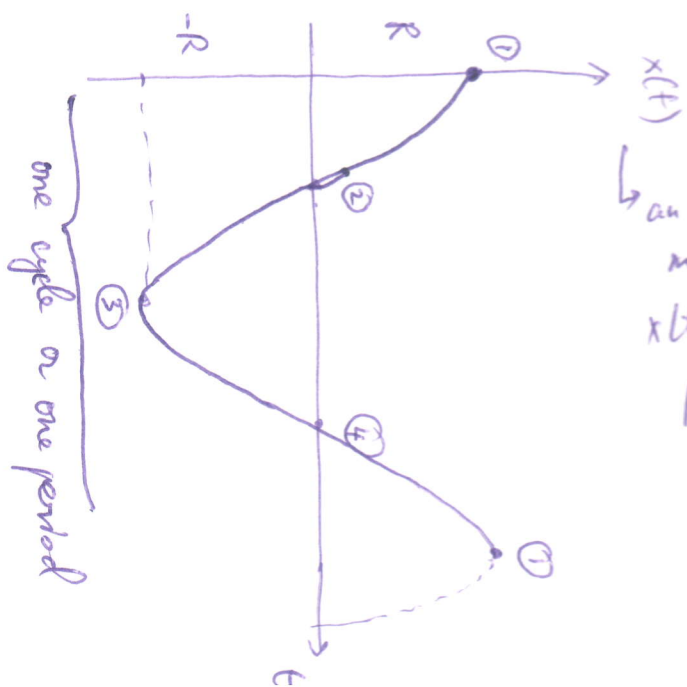
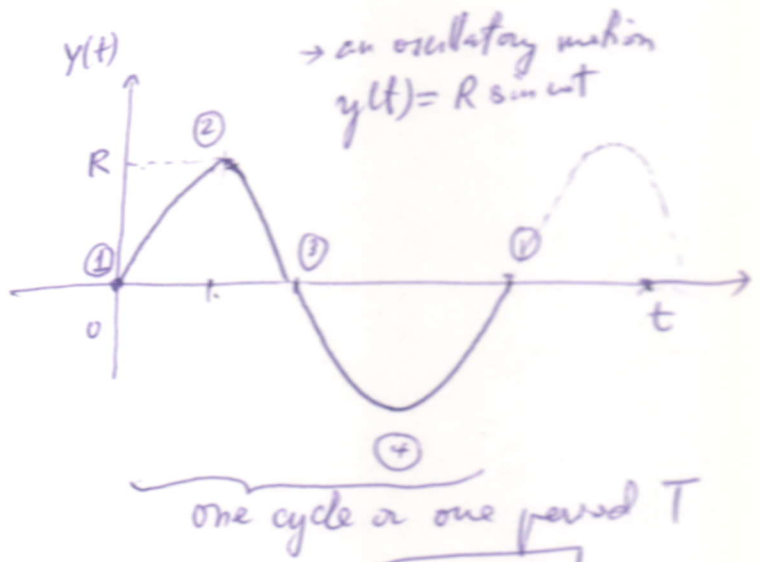
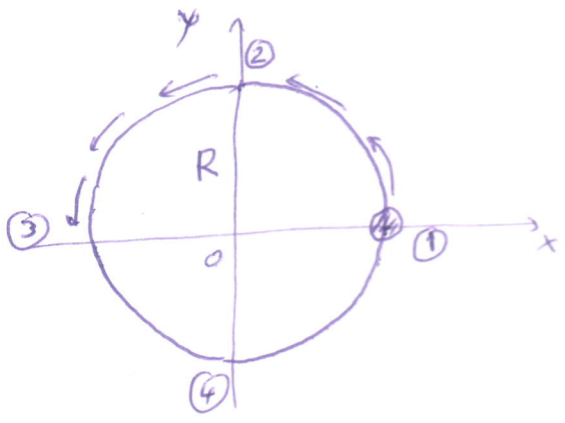
4) A particle trapped in a potential well



→ Assume there is no friction
 Simple Harmonic Motion
 $x(t) = x_m \cos(\omega t)$ → Motion SHM
 → If there is friction: damped oscillatory motion:
 $x(t) = x_m e^{-\frac{bt}{2m}} \cos(\omega t + \phi)$
 amplitude decaying exponentially

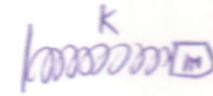
5) Coordinate x & y of a particle undergoing a Uniform Circular

Motion or UCM:



→ an oscillatory motion
 $x(t) = R \cos(\omega t)$ (x & y or coords of a particle in UCM) → are shifted by a phase of 90° or $\frac{\pi}{2}$

$$T = \frac{2\pi}{\omega}$$

Summary: For a spring & bob: 

SHM: $\frac{d^2x}{dt^2} = -\frac{k}{m}x$ (x : position of mass m)

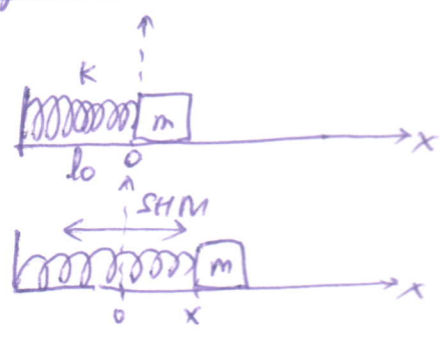
↳ Solution is $x(t) = x_m \cos \omega t$; $\omega = \sqrt{\frac{k}{m}}$

Damped SHM: $\frac{d^2x}{dt^2} = -\frac{k}{m}x - \frac{b}{m} \frac{dx}{dt}$

damping term $-\frac{b}{m} \frac{dx}{dt}$

↳ Solution is $x(t) = x_m e^{-\frac{bt}{2m}} \cos(\omega t + \phi)$

Energy in SHM: For a spring & bob



SHM = $x(t) = x_m \cos \omega t$
 ↳ displacement wrt. equilibrium length
 $\omega = \sqrt{\frac{k}{m}}$

Total energy: since system laying on a horizontal surface
 → same grav. potential energy at all times
 → can ignore.

↳ $E = KE + U_{elastic} = \underbrace{\frac{1}{2}mv^2}_{\text{mass } m} + \underbrace{\frac{1}{2}kx^2}_{\text{spring } k}$

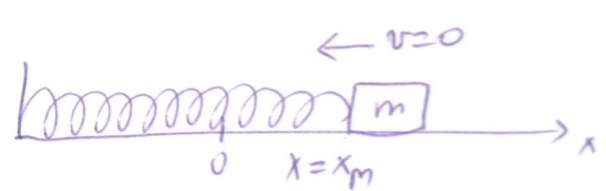
SHM: $\left\{ \begin{array}{l} x(t) = x_m \cos \omega t \\ v(t) = \frac{dx}{dt} = -x_m \omega \sin \omega t \end{array} \right\} \rightarrow E = \frac{1}{2} m x_m^2 \omega^2 \sin^2 \omega t + \frac{1}{2} k x_m^2 \cos^2 \omega t$

$$\omega = \sqrt{\frac{k}{m}} \rightarrow \omega^2 = \frac{k}{m}$$

$$E = \frac{1}{2} m \dot{x}_m^2 + \frac{1}{2} k x_m^2$$

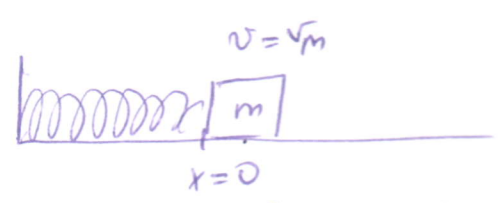
$$= \frac{1}{2} k x_m^2 \left[\sin^2 \omega t + \cos^2 \omega t \right]$$

Total energy in a mass + spring system is constant over time! equal to $\frac{1}{2} k x_m^2$. in SHM



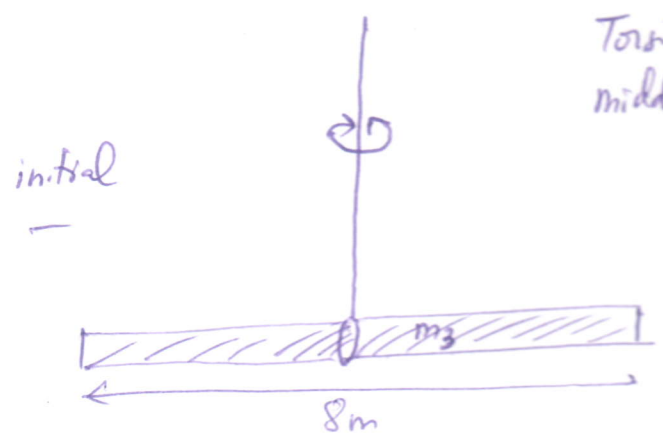
$$E = \frac{1}{2} m v^2 + \frac{1}{2} k x^2$$

$$E = \frac{1}{2} m 0^2 + \frac{1}{2} k x_m^2 = \frac{1}{2} k x_m^2$$

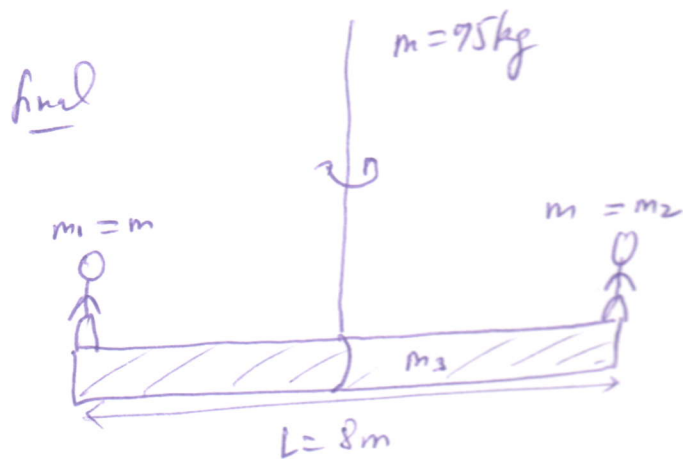


$$E = \frac{1}{2} m v_m^2 + \frac{1}{2} k 0^2 = \frac{1}{2} m x_m^2 \omega^2 = \frac{1}{2} m x_m^2 \frac{k}{m} = \frac{1}{2} k x_m^2$$

13.50



Torsional oscillations about middle axis. $\rightarrow \omega_i = \sqrt{\frac{K}{I_i}}$



$$\omega_f = \sqrt{\frac{K}{I_f}}$$

K : material of string torsional constant
 $\rightarrow K_i = K_f = K$

$$I_f = I_i + 2m\left(\frac{L}{2}\right)^2$$

$$I_f > I_i \rightarrow \omega_f < \omega_i$$

$$\frac{\omega_f}{\omega_i} = 0.8 = \frac{\sqrt{\frac{K}{I_f}}}{\sqrt{\frac{K}{I_i}}} = \sqrt{\frac{I_i}{I_f}}$$

ω_f diminishes by 20% $\omega_f = \omega_i - 0.2\omega_i = 0.8\omega_i$

When there is a square-root \rightarrow square up both sides

$$0.8^2 = \frac{I_i}{I_f} = \frac{I_i}{I_i + m\frac{L^2}{2}}$$

$$0.8^2 I_i + mL^2 \frac{0.8^2}{2} = I_i$$

$$I_i = \frac{mL^2 \frac{0.8^2}{2}}{1 - 0.8^2}$$

Also: $I_i =$ moment of inertia of a beam w.r.t. center axis: $I_i = \frac{1}{12} m_3 L^2$

$$\rightarrow \frac{1}{12} m_3 L^2 = m \frac{L^2}{2} \frac{0.8^2}{1 - 0.8^2}$$

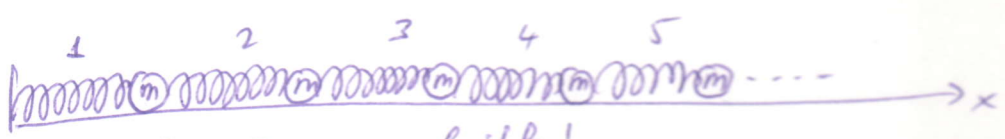
$$m_3 = 6m \frac{0.8^2}{1 - 0.8^2} = 450 \frac{0.8^2}{1 - 0.8^2}$$

$$m_3 = 800 \text{ kg}$$

Ch14 Wave Motion

Wave \neq oscillation

Wave: a propagation of a local oscillation (or disturbance)
(Note: not a propagation of matter!)



Masses of spring are negligible!

If an oscillation is started on spring #1, at that moment spring #5 is not yet affected: it takes some time for an oscillation or disturbance to propagate a certain distance

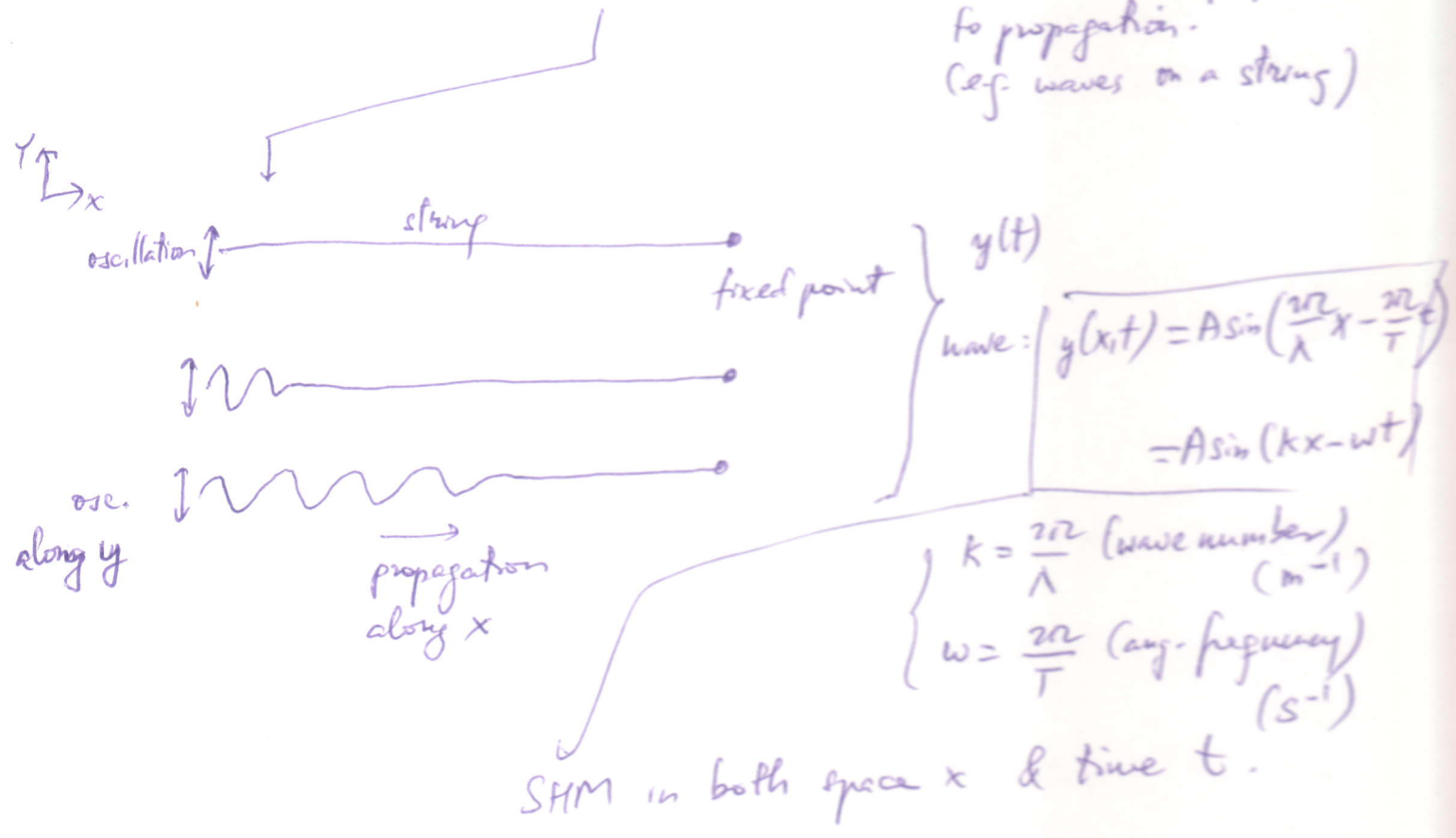
Observations:

1) Propagation is not instantaneous: propagation speed v
 is $v = \frac{\lambda}{T}$ ($\lambda = \text{lambda} = \text{wavelength} \rightarrow \text{space sep. b/w 2 consecutive peaks}$)
 $T = \text{period: time separation b/w 2 consecutive peaks}$

2) ~~Oscillations~~ ^{Masses & springs} are local, only the oscillation is propagated

3) Propagation is over a distance (in space) } both are SHM
 Oscillation is over a time (in time) }
 in a wave we have SHM both in time & in space

Waves → 2 types:
 { longitudinal waves : oscillations in same direction as propagation (e.g. springs & waves above)
Transverse waves : oscillations are perpendicular to propagation. (e.g. waves on a string)



13.45

pendulum → SHM → $\omega = \sqrt{\frac{g}{L}}$, L: pendulum length

↓ in a rocket

a) Rocket @ rest → $T_a = \frac{2\pi}{\omega} = \frac{2\pi}{\sqrt{\frac{g}{L}}}$
 ↓ $a = 0$

b) Rocket accelerating upward $a = \frac{g}{2}$ → $\vec{a} = \frac{g}{2} \hat{j}$
 $\vec{g} = -g \hat{j}$



$$T_b = \frac{2\pi}{\sqrt{\frac{|\vec{a} + \vec{g}|}{L}}} = \frac{2\pi}{\sqrt{\frac{|\frac{3g}{2} \hat{j}|}{L}}} = \frac{2\pi}{\sqrt{\frac{3g}{2L}}} = \frac{2\pi}{\sqrt{\frac{3g}{2L}}}$$

* Recall... when elevator accelerates upward, person feels heavier

→ $\vec{a} - \vec{g}$

$$T_b = \sqrt{\frac{2}{3}} \cdot \frac{2\pi}{\sqrt{\frac{g}{L}}} = \sqrt{\frac{2}{3}} T_a$$

(shorter period) (Period = time for one full swing)



c) Rocket acc. downward = $a = \frac{g}{2} \rightarrow \left. \begin{aligned} \vec{a} &= -\frac{g}{2} \hat{j} \\ \vec{g} &= -g \hat{j} \end{aligned} \right\}$

$\begin{matrix} y \\ \uparrow \\ x \end{matrix}$

$$T_c = \frac{2\pi}{\sqrt{\frac{|\vec{a} - \vec{g}|}{L}}} = \frac{2\pi}{\sqrt{\frac{|(-\frac{g}{2}) - (-g)|}{L}}} = \frac{2\pi}{\sqrt{\frac{|\frac{g}{2}|}{L}}}$$

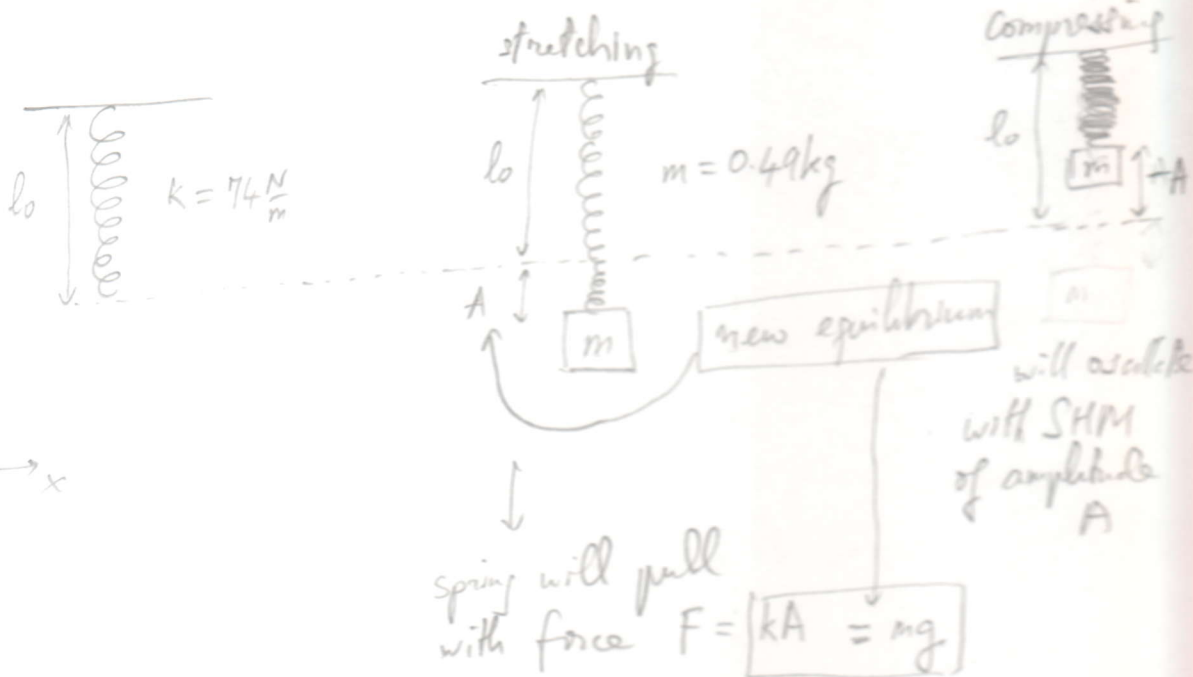
$$= \frac{2\pi}{\sqrt{\frac{g}{2L}}} = \sqrt{2} \frac{2\pi}{\sqrt{\frac{g}{L}}} = \sqrt{2} T_a \text{ (longer period)}$$

d) Rocket in free fall (downward) $a = g \rightarrow \left. \begin{aligned} \vec{a} &= -g \hat{j} \\ \vec{g} &= -g \hat{j} \end{aligned} \right\}$

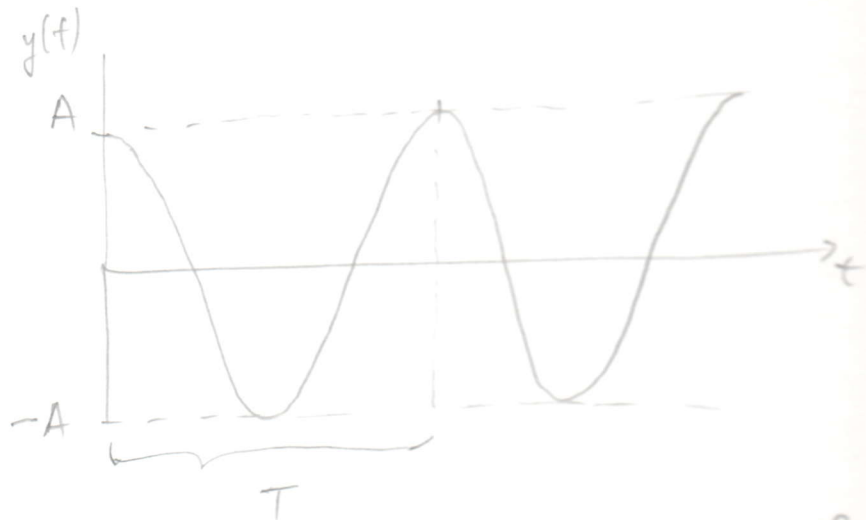
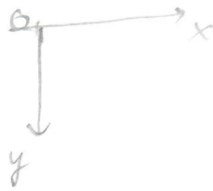
$$T_d = \frac{2\pi}{\sqrt{\frac{|\vec{a} - \vec{g}|}{L}}} = \frac{2\pi}{\sqrt{\frac{|(-g) - (-g)|}{L}}} = \frac{2\pi}{0} = \infty$$

(infinite period)
↓
pendulum stops.

13.64



a)



$$A = \frac{mg}{k} = \frac{0.49 \times 9.8}{74} = 0.065 \text{ m}$$

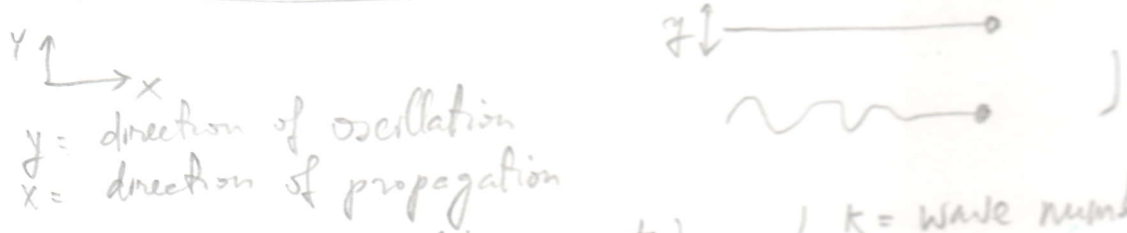
b)

Period of SHM for the spring & mass?

$$T = \frac{2\pi}{\omega} = \frac{2\pi}{\sqrt{\frac{k}{m}}} = 2\pi \sqrt{\frac{m}{k}} = 2\pi \sqrt{\frac{0.49}{74}} = 0.5 \text{ s}$$

Ch 14 Wave Motion (Cont.)

Transverse wave: (eg. wave along a string)

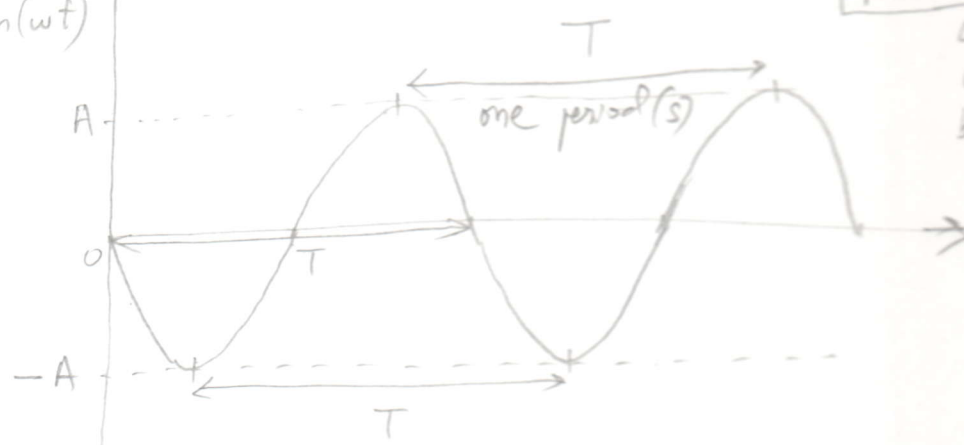


$$y(x, t) = A \sin(kx - \omega t)$$

- $k =$ wave number $= \frac{2\pi}{\lambda} (\text{m}^{-1})$
- $\lambda =$ wave length (m)
- $\omega =$ angular frequency (s^{-1})
- $= \frac{2\pi}{T}$
- $T =$ period (s)
- $A =$ amplitude (m)

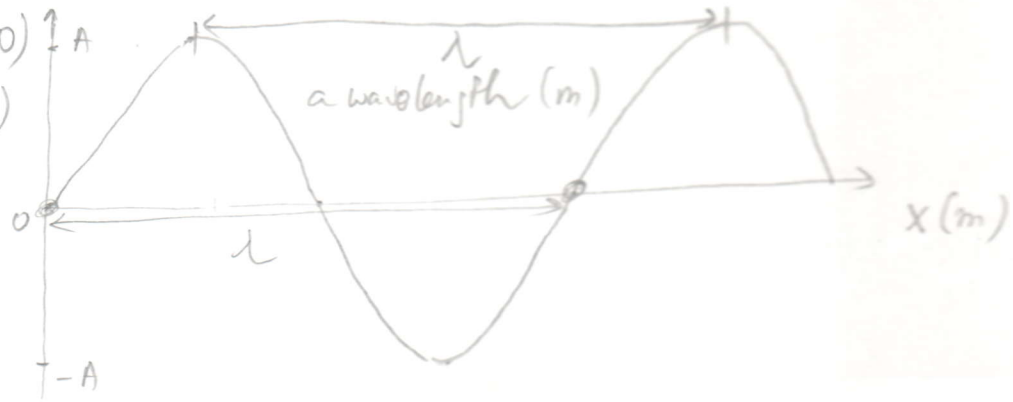
$$\sin(-\omega t) = -\sin(\omega t)$$

$$y(0, t) = -A \sin(\omega t)$$

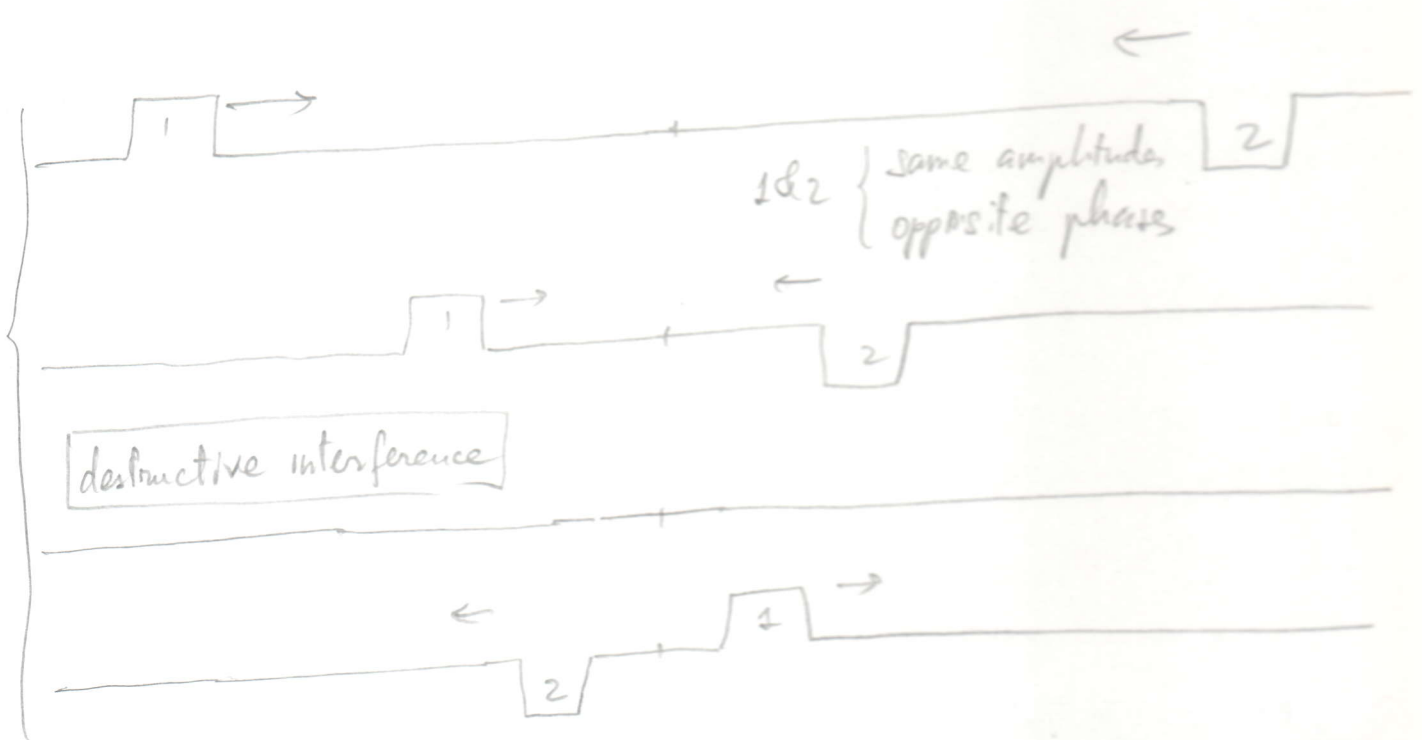
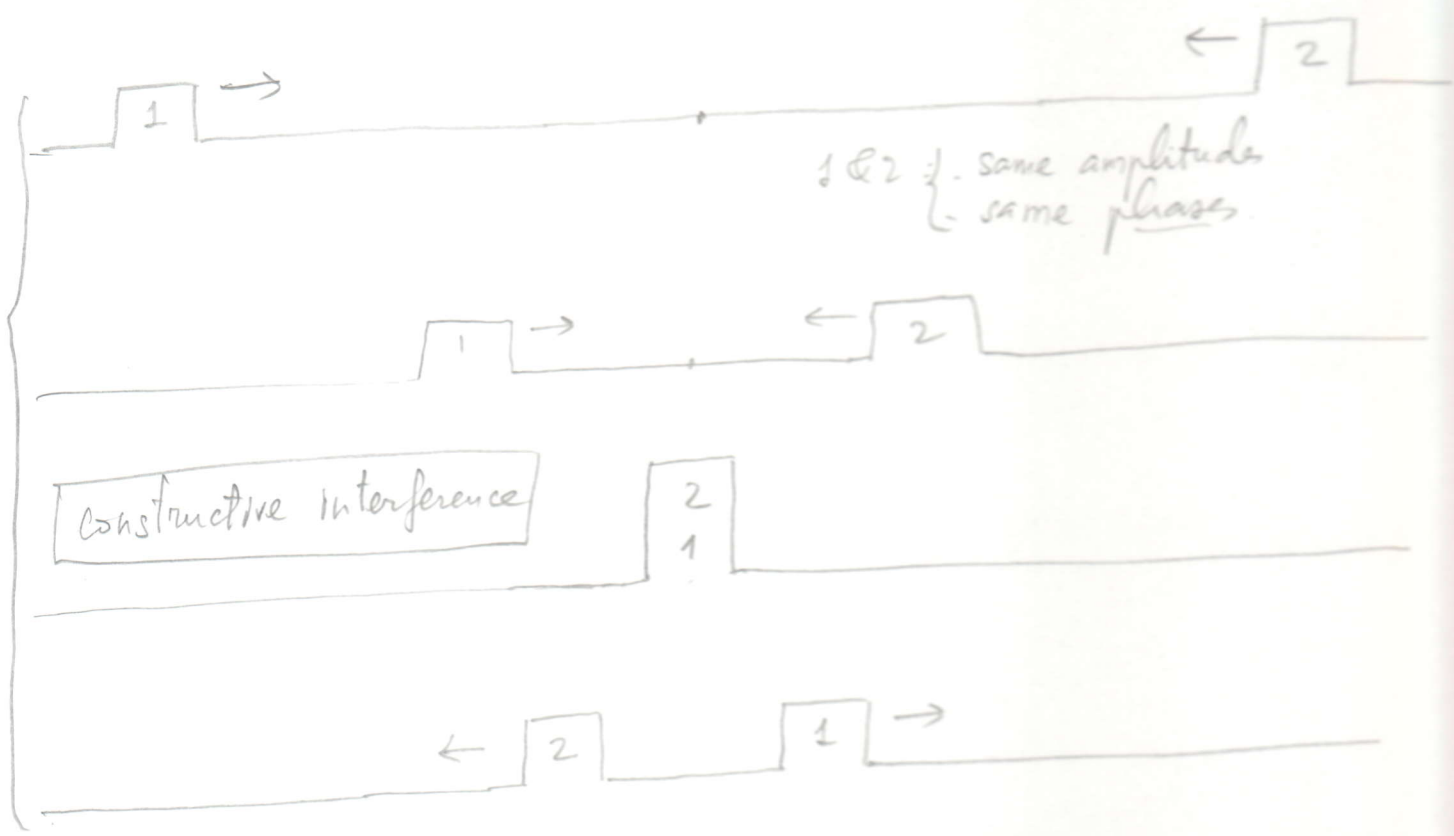


Period T: time separation b/w consecutive peaks or troughs or b/w two similar zeros of function increasing or decreasing

$$y(x, 0) = A \sin(kx)$$



Wave Superposition = (1+1 is NOT always 2)



How about a quantitative expression for a wave superposition or interference?

Transverse wave = $y(x,t) = A \sin(kx - \omega t)$

Superposition or interference of 2 waves coinciding at $x=0$ (e.g. midpoint in earlier visualization). To be more interesting the two waves will have different frequencies:

$\omega_1, \omega_2 \rightarrow \begin{cases} y_1(0,t) = A \sin(-\omega_1 t) \\ y_2(0,t) = A \sin(-\omega_2 t) \end{cases}$

$y_1(0,t) + y_2(0,t) = -A [\sin \omega_1 t + \sin \omega_2 t]$

Trig. identity: $\sin \alpha + \sin \beta = 2 \sin(\frac{\alpha + \beta}{2}) \cos(\frac{\alpha - \beta}{2})$

$= -2A [\sin(\frac{\omega_1 + \omega_2}{2} t) \cdot \cos(\frac{\omega_1 - \omega_2}{2} t)]$

allows us to describe a real situation:

When ω_1 & ω_2 are close ($\omega_1 = 1000 \frac{rad}{s}$ & $\omega_2 = 1004 \frac{rad}{s}$)

- ↳ Average \sim either one
- ↳ Difference \sim much smaller than either frequency
- ↳ This imposes a very slow modulation on the amplitude of the combined wave

$y_1(0,t) + y_2(0,t) = \underbrace{-2A \cos(\frac{\omega_1 - \omega_2}{2} t)}_{\text{slowly modulated}} \underbrace{\sin(\frac{\omega_1 + \omega_2}{2} t)}_{\text{similar to either}}$

Practical applications of thro slowly modulated amplitude

BEAT PHENOMENON :

- 1) Tuning of string instrument
- 2) Maintenance of turbo (helix) aircrafts.

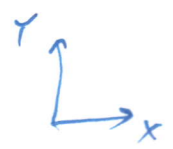
(one helix on each wing = three engines
supposed to generate exact same frequencies.

High rpm → high frequency sound → we hear
flat noise from each engine.

When both engines are on, we hear oscillations,
which are actually the beats b/w the two
sounds.

14.54

Wave in a wire : $y(x,t) = 1.5 \sin(0.1x - 560t)$



oscillation along y
propagation along x

Transverse wave:

$$y(x,t) = A \sin(kx - \omega t)$$

- a) Amplitude $A = 1.5 \text{ cm}$
- b) Wave number $k = 0.1 \text{ cm}^{-1} = \frac{2\pi}{\lambda} \rightarrow \lambda = \frac{2\pi}{0.1 \text{ cm}^{-1}} = 62.8 \text{ cm.}$
- c) Period $T = \frac{2\pi}{\omega} = \frac{2\pi}{560} \text{ s} = 11.2 \times 10^{-3} \text{ s} = 11.2 \text{ ms}$
- d) Wave speed: $v = \frac{\lambda}{T} = \frac{62.8 \times 10^{-2} \text{ m}}{11.2 \times 10^{-3} \text{ s}} = 56 \text{ m/s}$
- e) Power carried by the wave: $\bar{P} = \frac{1}{2} \mu \omega^2 A^2 v$

- μ : linear density of the wire
- ω : ang freq. of the wave
- A : amplitude of wave
- v : wave speed

μ is not given, but the tension in the wire is $T = 28 \text{ N}$

Transverse wave in a wire = $v = \sqrt{\frac{T}{\mu}} \rightarrow \mu = \frac{T}{v^2}$

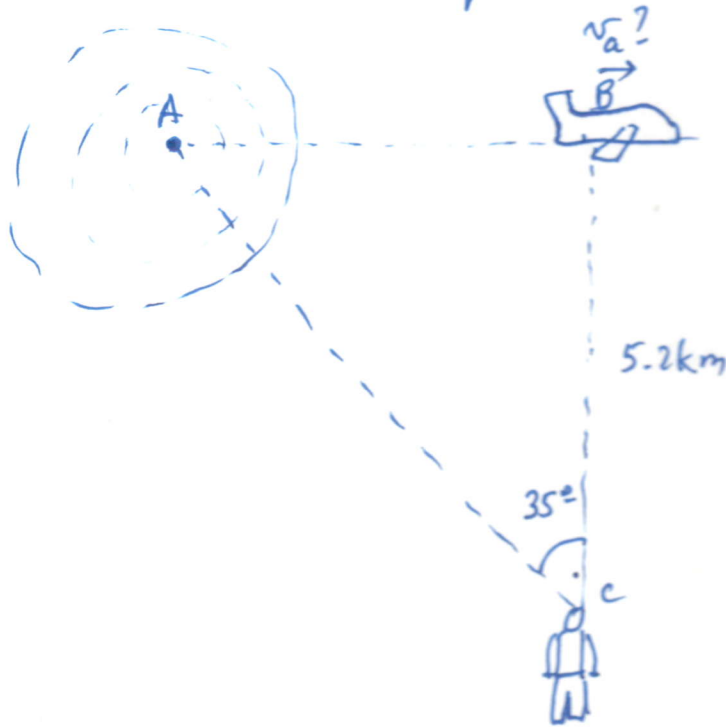
$$\bar{P} = \frac{1}{2} \frac{T}{v} \omega^2 A^2 v = \frac{1}{2} \frac{T \omega^2 A^2}{v} = \frac{1}{2} \frac{28 \times 560^2 \times 0.015^2}{56} \text{ W}$$

$$\bar{P} = \cancel{35.28} \text{ W} = \frac{1}{2} 28 \times 5600 \times 0.015^2 = 14 \times 0.15^2$$

$$\bar{P} = \cancel{0.315} \text{ W} = 17.4 \text{ W}$$

4.61

Sound wave takes some time to reach you, in the same time the airplane has continued along its path.



$v_{\text{sound}} = 330 \text{ m/s}$ (in water)

Not saying the contrary: \rightarrow Airplane is traveling at constant speed $v_a = \frac{AB}{t}$; $t =$ time for sound wave to propagate from A to C

$$t = \frac{AC}{v_{\text{sound}}}$$

$$\begin{aligned}
 \hookrightarrow v_a &= \frac{AB}{\frac{AC}{v_{\text{sound}}}} = \frac{AB}{AC} v_{\text{sound}} \\
 &= \sin 35^\circ v_{\text{sound}} \\
 &= 330 \sin 35^\circ = 189 \text{ m/s}
 \end{aligned}$$

(14.27)

Transverse wave :

$$\begin{cases} A = 3 \text{ cm} = 0.03 \text{ m} \\ \lambda = 0.75 \text{ m} \\ v = 6.7 \text{ m/s} \end{cases}$$

↳ on a stretched spring : $\mu = 0.17 \text{ kg/m}$ → linear mass density

Find spring tension T :

For a transverse wave in a string : $v = \sqrt{\frac{T}{\mu}} \rightarrow T = \mu v^2$

↓
wave speed

$$= 0.17 \times 6.7^2$$

$$\boxed{T = 7.63 \text{ N}}$$

→ The other given data (A, λ) would be useful to calculate ω, \bar{P}

Ch 14 Wave Motion (Cont.)

Standing waves:

- string along x, at length L it is attached to a fixed point.
- perturb free end at origin by moving it up & down.
- this generates a wave that propagates in +x



Wave gets reflected, or receives a phase shift of 180°



incoming + reflected

- @ L the wave gets reflected w/c of the fixed point
- if you keep sending in waves by perturbing the free end; the incoming wave gets combined with the reflected wave. → formation of standing waves: its particular shape depends on how fast you perturb the free end.

Math description:

$$\begin{aligned}
 y_T(x,t) &= \underbrace{y_1(x,t)}_{\text{incoming wave}} + \underbrace{y_2(x,t)}_{\text{reflected wave}} \\
 &= A \cos(kx - \omega t) - A \cos(kx + \omega t) \\
 &\quad \downarrow \text{propagation in } +x \quad \downarrow \text{propagation in } -x
 \end{aligned}$$

$$y_T(x,t) = A \left[\underbrace{\cos(kx - \omega t)}_{\alpha} - \underbrace{\cos(kx + \omega t)}_{\beta} \right]$$

Trig. identity: $\cos \alpha - \cos \beta = -2 \sin \frac{\alpha + \beta}{2} \sin \frac{\alpha - \beta}{2}$

$$\rightarrow y_T(x,t) = -2A \sin\left(\frac{kx - \omega t + kx + \omega t}{2}\right) \sin\left(\frac{kx - \omega t - kx - \omega t}{2}\right)$$

$$\boxed{y_T(x,t) = 2A \sin kx \sin \omega t} \quad (\text{incoming + reflected wave.})$$

We need to incorporate the fact that $\boxed{y_T(x=L,t) = 0}$
 (fixed point @ $x=L$)

$$\downarrow \quad \underbrace{2A}_{\neq 0} \sin kL \underbrace{\sin \omega t}_{\neq 0} = 0 \quad \text{at all } t \Rightarrow \sin kL = 0$$

\Rightarrow what non zero values for kL would give me $\sin kL = 0$

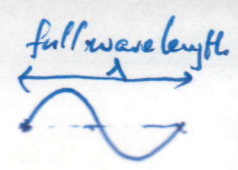
$$\hookrightarrow kL = n\pi \quad (n = 1, 2, 3, \dots)$$

$$\frac{2\pi}{\lambda} L = n\pi$$

$$\rightarrow \boxed{\lambda = \frac{2L}{n} \quad (n = 1, 2, 3, 4, \text{etc.})}$$

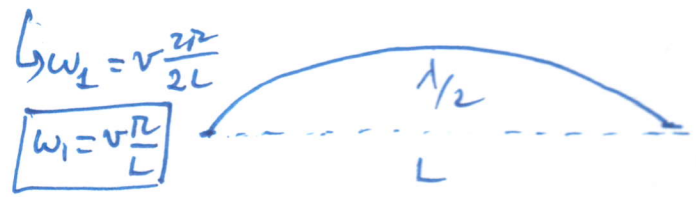
Possible wavelengths for standing waves in a string of length L :

$$\lambda_1 = 2L; \lambda_2 = L; \lambda_3 = \frac{2L}{3}; \lambda_4 = \frac{L}{2}; \text{etc.}$$

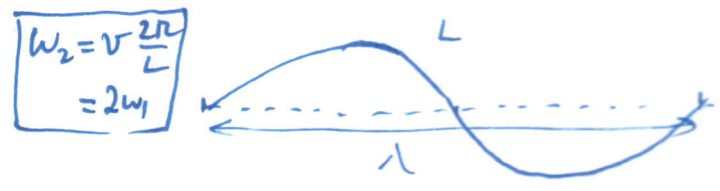


What do standing waves look like?

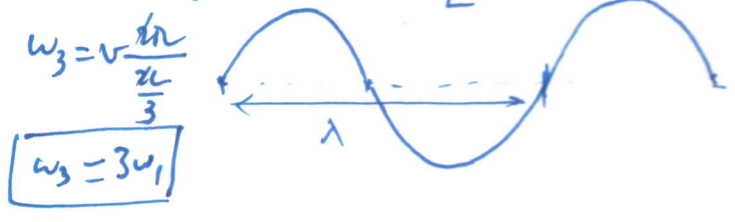
$\lambda_1 = 2L \rightarrow$ in L there is half a wave length



$\lambda_2 = L$



$\lambda_3 = \frac{2L}{3}$



→ Showed standing waves movie.

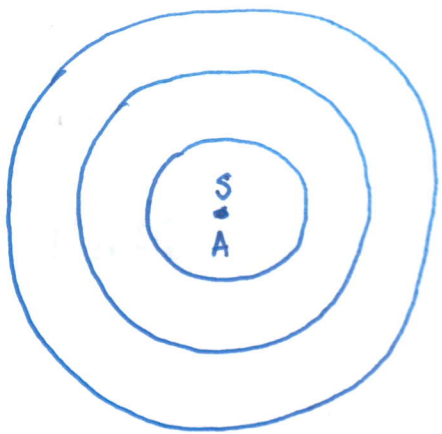
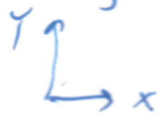
Derivation of wave speed: $v = \frac{\lambda}{T} = \frac{\frac{2\pi}{k}}{\frac{2\pi}{\omega}} = \frac{\omega}{k}$

Alternative derivation: $v = \frac{\lambda}{T} = \frac{\lambda}{\frac{\lambda}{v}} = v$

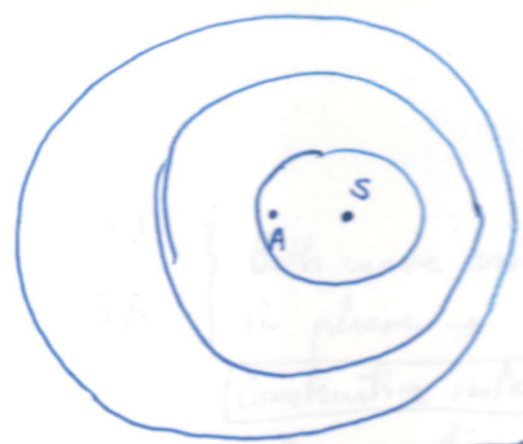
Final boxed equation: $\omega = vk = v \frac{2\pi}{\lambda}$

... wave A ...
... both waves have ...
... identical. Since ...
... wave B is out ...

Doppler Effect : moving source



source @ rest



wavefronts are further from each other

sounds from a leaving train have a longer effective wavelength

$$\lambda' = \lambda + uT$$

receding

$$f' = \frac{f}{1 + \frac{u}{v}}$$

receding source

wavefronts are closer together

sounds from a coming train will have an effective shorter wavelength

$$\lambda' = \lambda - uT$$

approaching

source speed
wavelengths when source was static.

$$f' = \frac{f}{1 - \frac{u}{v}}$$

approaching

Period of sound wave

u = source speed
v = wave speed
f = original frequency of sound when source was static.